

# Physics of the SOL Heat Load Scale: Stability and Turbulence Spreading

<sup>1</sup>Xu Chu, <sup>2</sup>P. H. Diamond

<sup>1</sup> University of Chinese Academy of Sciences, Beijing 100049, China

<sup>2</sup> University of California San Diego, La Jolla, California 92093, USA

Email: [chuxu17@mailsucas.ac.cn](mailto:chuxu17@mailsucas.ac.cn)

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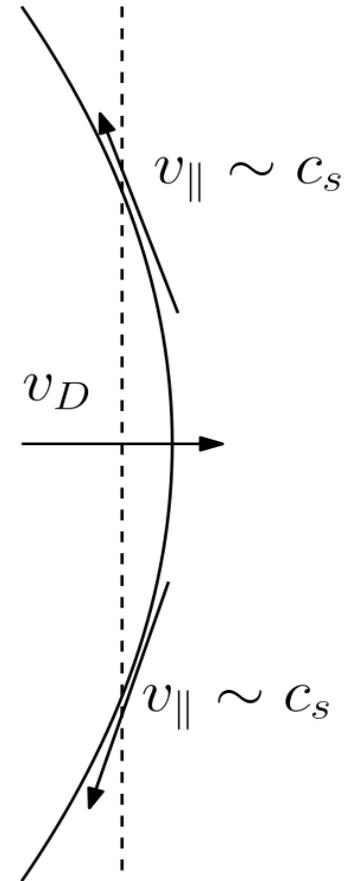
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# The Problem: Small SOL Width for Current Day H-mode discharges

- Goldston's Scaling: 2012, Goldston, *Nucl. Fusion*
  - $\lambda = v_D \tau_{\parallel} = \rho_{\theta} \epsilon \sim B_{\theta}^{-1}$

Note:

- Based on drifts, no turbulent transport
- Size independent
- Produce very narrow  $\lambda$
- Small layer for large device with high current



# Outline – Overview of the Talk

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- SOL stable due to  $E \times B$  shear and sheath resistivity:
  - Point to Turbulent Spreading from Pedestal
- Influence of Spreading: 2Box model: Pedestal  $\rightarrow$  SOL
  - SOL as a flux ( $Q, \Gamma_n, \Gamma_e$ ) driven Boundary Layer  $\Gamma_e$ : Turbulence Intensity Flux
  - $\Gamma_e$  from pedestal: Spreading with shearing
- **New Trade Off: Layer Broadening *v. s.* Confinement (Can turbulent pedestal broaden  $\lambda$  while maintaining adequate confinement?)**
  - SOL width  $\lambda$  as a function of  $\Gamma_e$
  - Estimate Minimal level of Pedestal Fluctuation Needed to Broaden the SOL (Scaling)
- Implication for HDL and H $\rightarrow$ L back transition



Why does Goldston's Scaling Work?  
SOL  $E \times B$  shearing  $\sim \lambda^{-2}$

# Linear Analysis: SOL Stability

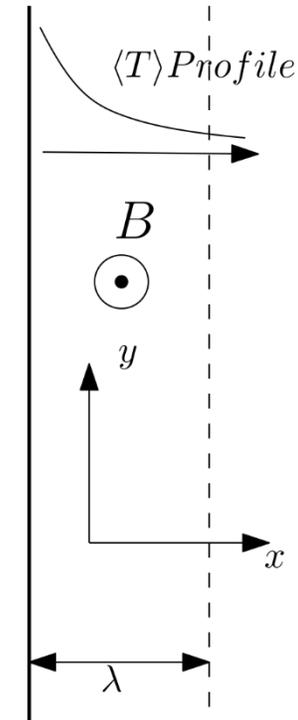
Model: (Linear Perturbation of the model by Myra. et. al. 2002):

$$\begin{cases} \partial_t \Delta \delta \phi + \lambda_T \omega_s e^{-x/\lambda_T} \partial_y \Delta \delta \phi - e^{-x/\lambda_T} \beta \partial_y \delta n \\ \quad = \alpha e^{x/2\lambda_T} \delta \phi + \nu \Delta^2 \delta \phi \\ \partial_t \delta n + \lambda_T \omega_s e^{-x/\lambda_T} \partial_y \delta n + \partial_y \delta \phi \partial_x \ln n_0 \\ \quad = D \Delta \delta n / n + 2D \partial_x \ln n_0 \partial_x \delta n \end{cases}$$

Note:

- $\beta = 2\rho/R$ . Usual: denoted by  $\beta_t$
- $E \times B$  Shearing Rate:  $\omega_s = \frac{3\langle T \rangle}{eB\lambda_T^2}$ , determined by the width

$$\gamma \approx c_s / \sqrt{\lambda R} - \omega_s$$



Small Heat Load Width

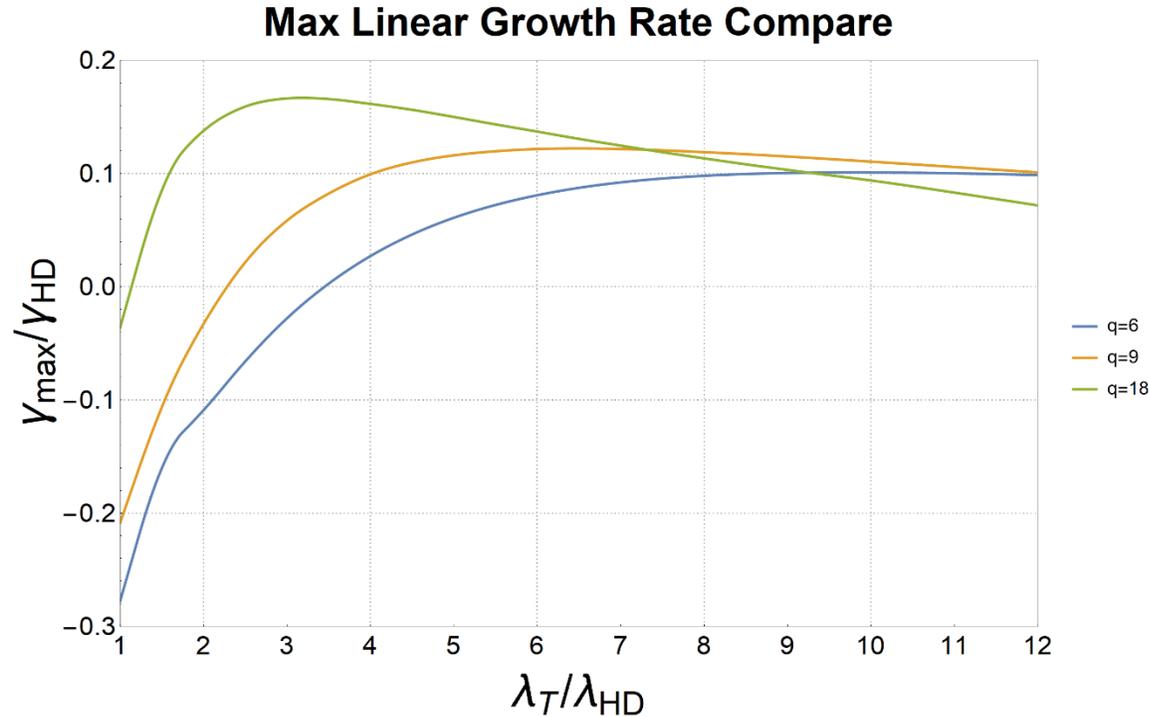


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# Linear Analysis: SOL Stability

Linear growth rate with neoclassical diffusion.

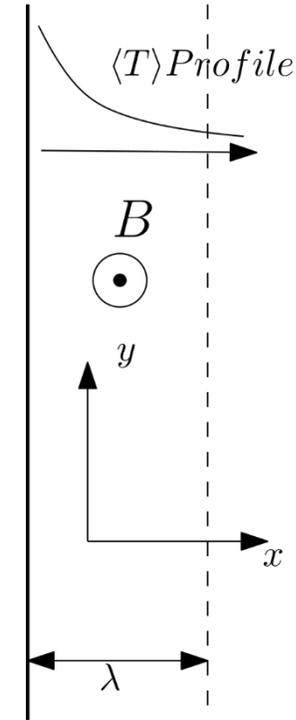


Interchange mode is stabilized by the combination of shear, sheath resistivity and plateau region diffusion:  
Goldston Scaling Works



Origin of SOL fluctuations:

- Local Instability  $\times$
- Spreading  $\sqrt{\quad}$



# Edge-SOL Connection Already Indicated

L mode: HL-2A Ting Wu, et. al., 2021, *Plasma Sci. Technol.*

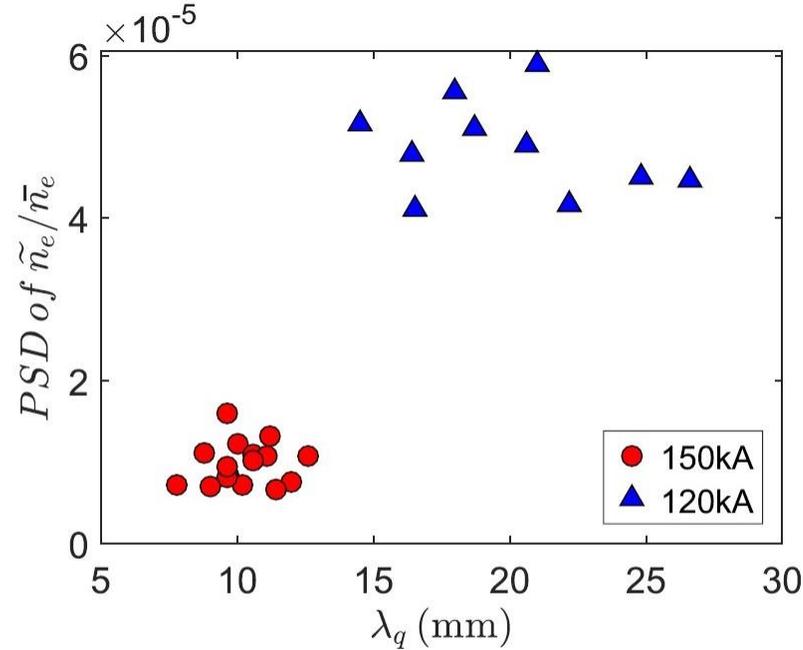
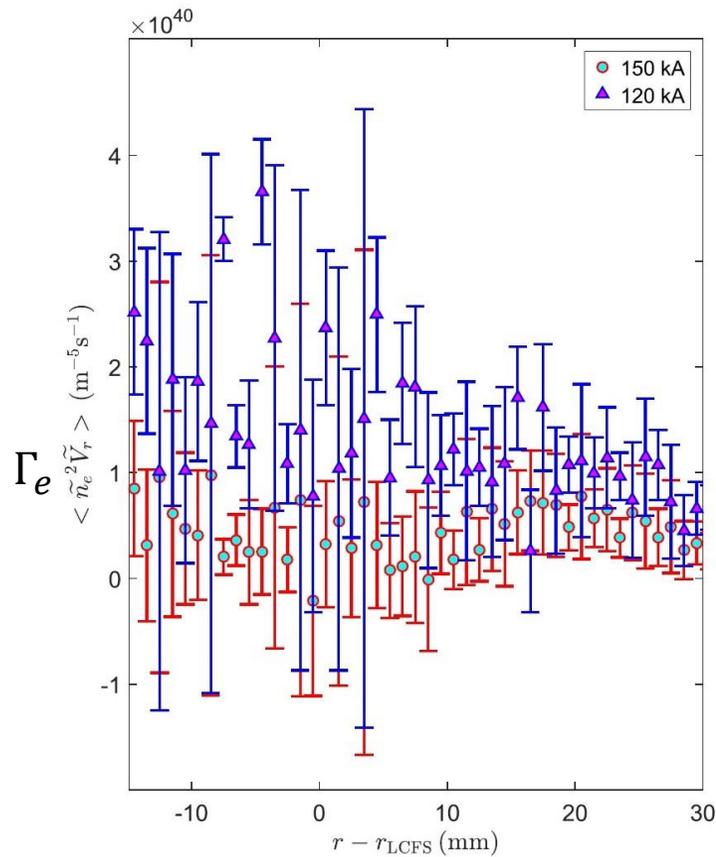


Figure 7. The power of relative density fluctuation level at  $r - r_{\text{LCFS}} \approx -15$  to  $-10$  mm versus SOL width with different plasma currents.

SOL width larger for stronger edge turbulence levels at lower current.

Suggests Inside turbulence  $\rightarrow$  SOL width influence due to spreading.

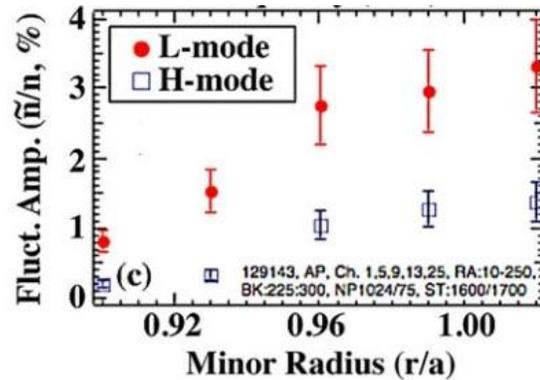
PSD  $\tilde{n}/n$  inside separatrix vs. SOL width

- Flux of turbulence energy into the SOL indicated
- Turbulence spreading reduced at larger current



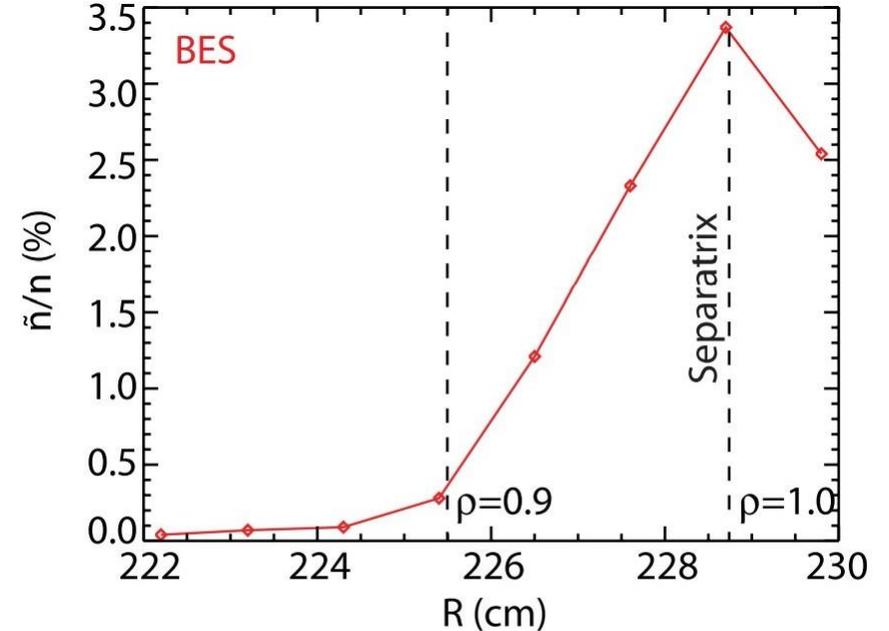
# Turbulence in Pedestal

- Reduced but Finite Fluctuation
  - Wide Pedestal QH Regime
  - Grassy ELM Regime
  - ...



**Figure 4.** Density fluctuation characteristics measured near the edge ( $0.9 < r/a \leq 1.0$ ) of an upper-single-null discharge: (a) frequency and time resolved spectrogram of density fluctuations at  $r/a = 0.95$  showing rapid fluctuation suppression at the L–H transition at  $t = 1696$  ms, (b) spectra of fluctuations before and after the L–H transition, (c) the integrated fluctuation amplitude edge profile in L and H-mode.

McKee, et. al., 2009, *Nucl. Fusion*



**Figure 9.** Radial profile of relative density fluctuations integrated over 10kHz through 80kHz from BES measurements around 4300 ms in discharge 163518.

Xi Chen, et. al., 2018, *Nucl. Fusion*

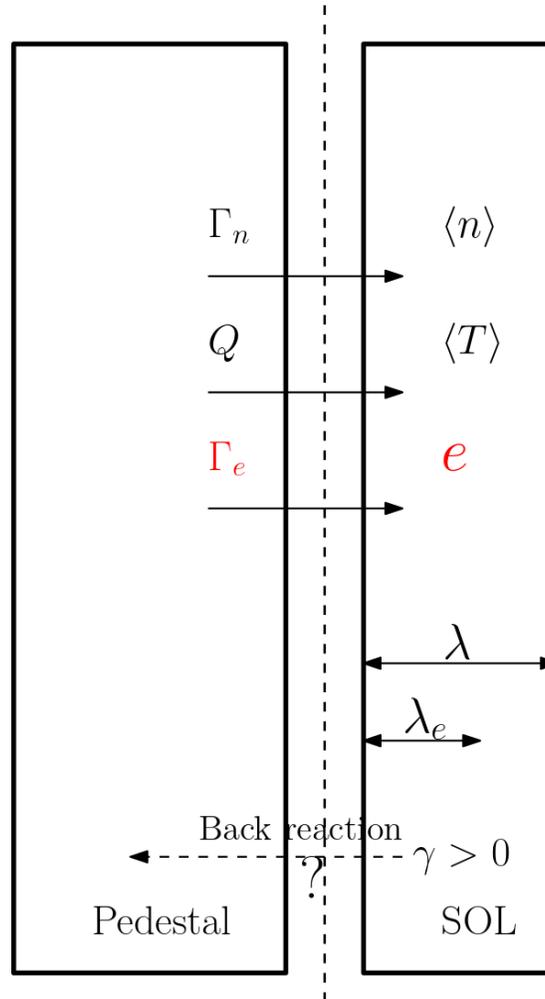


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# How Spreading Modifies SOL Width

# Spreading Model Overview

- Pedestal Model
  - Relating pedestal parameters to intensity flux
  - Intensity gradient combined with pedestal  $E \times B$  shear
  - Consider microturbulence and MHD (ballooning)



- SOL Model
  - SOL as a BL with multiple drives:  $Q, \Gamma_e$
  - Calculate  $\lambda$  from  $Q$  and  $\Gamma_e$
  - $\Gamma_e$  balances linear and nonlinear damping, determining  $\lambda$
  - $Q$  determines  $\langle T \rangle_{sep}$

$\Gamma_e$ : Turbulent Intensity Flux from Pedestal

New Trade off:  
Layer Broadening v.s. Confinement



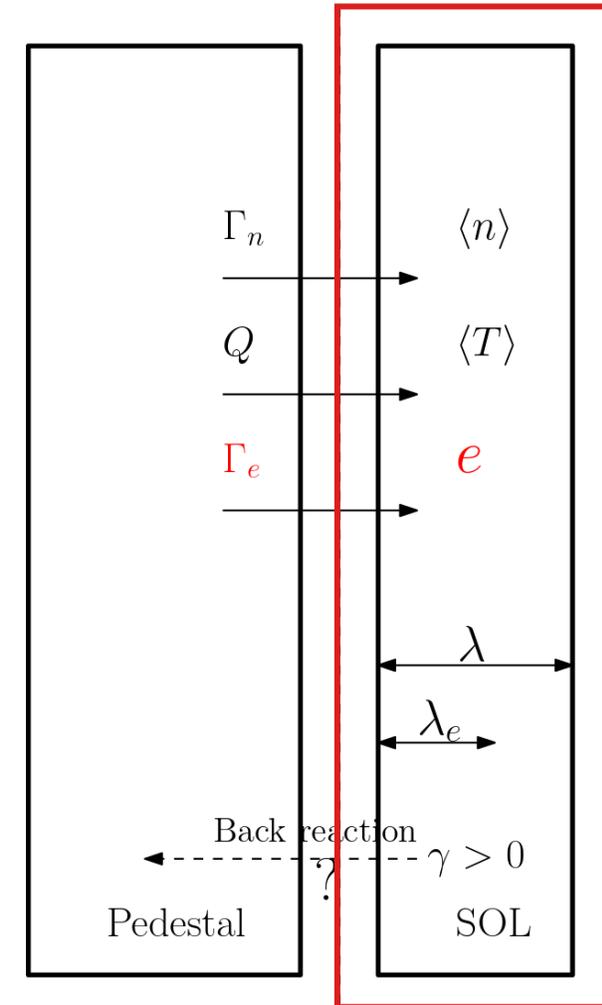
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# SOL Model: Theory

- Turbulent Intensity Equation: Hahm, Diamond, et. al.
  - $\partial_t e = \gamma e - \sigma e^{1+\kappa} - \partial_x \Gamma_e$ , Spatial 1D:  $e(x, t)$
- Integrate radially over the SOL
- Turbulent Energy Balance:
  - $\Gamma_{e0} = \lambda_e |\gamma| e + \sigma e^{1+\kappa} \lambda_e$
  - $\Gamma_{e0}$ : Intensity flux from pedestal (at the separatrix)

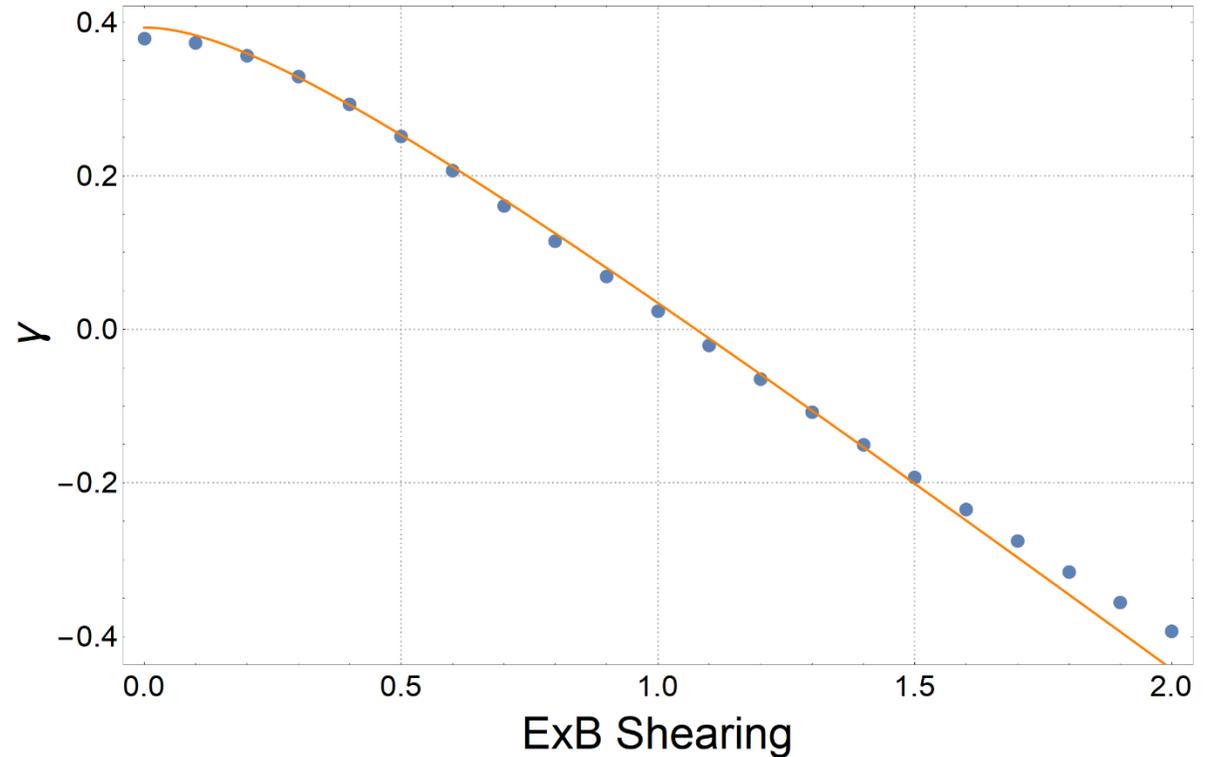
Note:

- No assumptions on the form of intensity flux
- Heat flux  $Q$  determines  $\langle T \rangle_{sep}$  and enters the model from  $c_s$  in  $\gamma_0$
- SOL as a BL with 2 drives ( $Q, \Gamma_e$ )



# SOL Model: Linear and Nonlinear Damping

- Linear Damping:
  - $\gamma = \gamma_0 - 3T_e/eB\lambda_T^2 \approx -3T_e/eB\lambda_T^2$
  - $\gamma_0 = c_s/\sqrt{R\lambda}$
- Nonlinear Damping:
  - General Form:  $\sigma e^{1+\kappa}$
  - Cascade:  $\kappa = 1/3$ ,  $\sigma = \alpha^{1/3}$  (One possibility)



Numerical Result of  $\gamma$  v. s.  $\omega_s$



# SOL $\lambda - \Gamma_e$ Relation: Unified Relation

- Account for both drift and  $\tilde{v}$

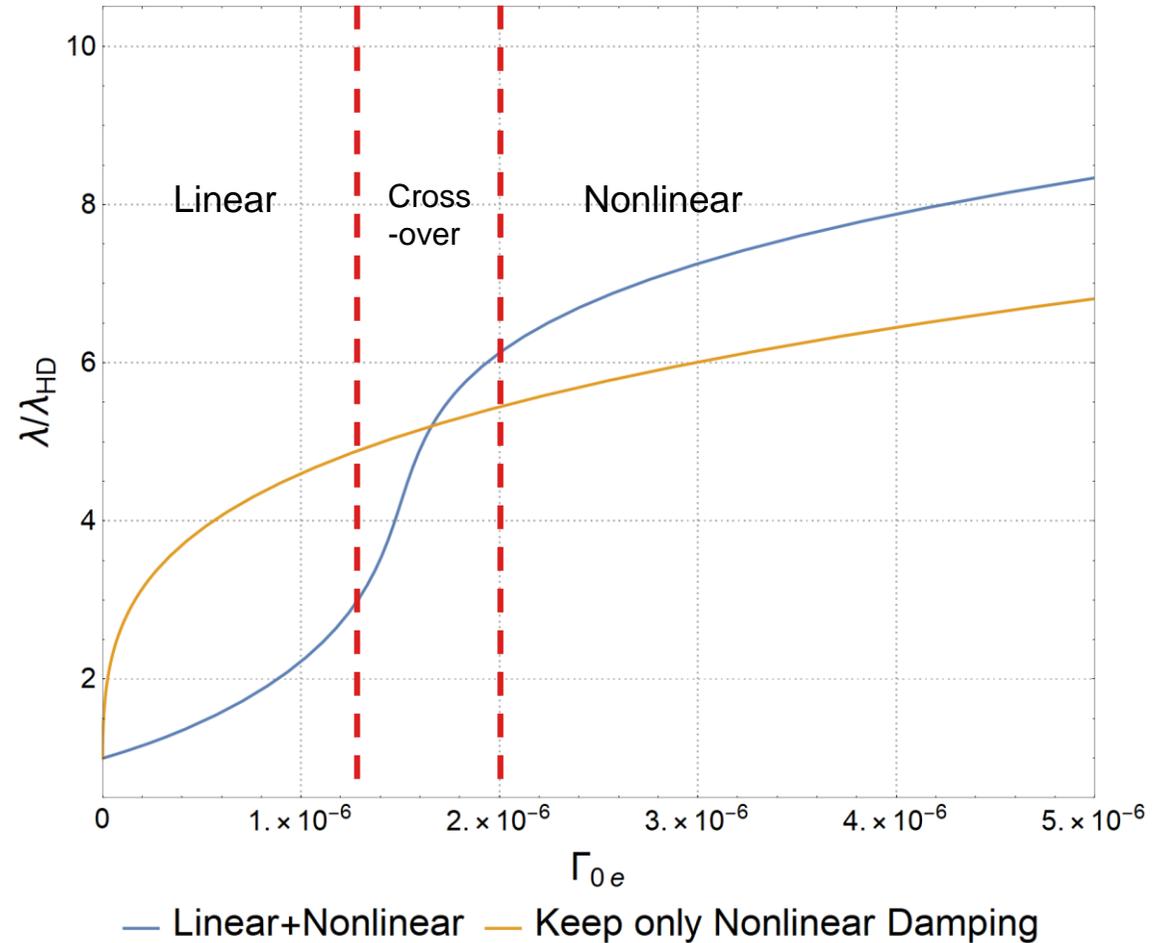
- $$\lambda_e = \lambda = \sqrt{\lambda_{HD}^2 + \tau_{\parallel}^2 e}$$

- $$\Gamma_{0e} = -\left(\sqrt{\beta/\lambda} - 3/\lambda^2\right)e\lambda + \sigma e^{1+\kappa}\lambda$$

↑ Linear Damping      ↑ Nonlinear Damping

Note:

- Shape of the curve is sensitive to linear and nonlinear damping



## The Cost –

How Strong Pedestal Fluctuation is needed to Broaden the Layer  
(Calculate  $\Gamma_{0e}$  from Pedestal)

# Pedestal Model: Spreading with $E \times B$ Shear

- $\Gamma_e = -\tau_c K \partial_x K$  (interpreted coarse grained)
- $\Gamma_{e0} \sim \tau_c K^2 / w_{ped}$
- Shearing( $\omega_s$ ) modifies  $\tau_c$ 
  - $\tau_c^{-1} = Dk^2(1 + \omega_s^2 \tau_c^2)$ 
    - Strong Shear Limit:  $\tau_c = (Dk^2)^{-1/3} \omega_s^{-2/3}$
  - $D = \int_0^\infty \langle v(0)v(\tau) \rangle d\tau = \int_0^\infty d\tau \sum_k |v_k|^2 e^{-k_y^2 \omega_s^2 D \tau^3 - k^2 D \tau}$  (Kubo formular)
    - Strong Shear Limit:  $D \sim |v|^{1.5} k^{-0.5} \omega_s^{-0.5}$
  - In strong shear limit:  $\tau_c = \tau_t^{0.5} \omega_s^{-0.5}$ ,  $\tau_t$  is eddy turnover rate, or the  $\tau_c$  when  $\omega_s = 0$ , denoted by  $\tau_{c0}$

$\tau_c$ : 3 processes

- Wave interaction
- Nonlinear Decorrelation
- Shearing:  $\omega_s$

Note: Strong shear reduces  $\tau_c$ , reflects transport barrier



# Estimation of Intensity Flux from Pedestal

- Drift Wave: (microturbulence)
  - $\Gamma \sim \tau_c K \partial_x K$ 
    - $K$ : turbulent kinetic energy
  - $\tau_{c0} v_* = \rho$
  - Weak Shear Limit:
    - $\Gamma_e \sim a \frac{L_n}{\Omega \rho} K^2 / w_{ped}$ ,  $a$  of  $O(1)$
  - In strong shear limit:
    - $\Gamma_e \sim a \left( \frac{L_n}{\Omega \rho} \right)^{0.5} \omega_s^{-0.5} K^2 / w_{ped}$

Analogue: Spreading of a turbulent spot

- Ballooning Mode: (MHD)
  - $\tilde{v} \sim \gamma \Delta_r = L_p \omega_A \left( \frac{L_{pc}}{L_p} - 1 \right)^{0.5} \frac{\Delta_r}{L_p}$ 
    - $L_p$  is estimated by pedestal width  $w_{ped}$
  - $\Gamma_e \sim \tau_c K^2 / w_{ped}$ ,  $\tau_{c0} \sim 1/\gamma$
  - Weak Shear Limit:
    - $\Gamma_e \sim \frac{1}{\gamma} (\gamma \Delta_r)^4 / w_{ped} \sim \omega_A^3 \left( \frac{L_{pc}}{L_p} - 1 \right)^{1.5} \Delta_r^4 / w_{ped}$
  - In strong shear limit:
    - $\Gamma_e \sim \omega_s^{-0.5} \omega_A^{3.5} \left( \frac{L_{pc}}{L_p} - 1 \right)^{1.75} \Delta_r^4 / w_{ped}$

$$E_r \approx \frac{\nabla p}{ne}, \omega_s \sim \frac{\rho^2 \Omega}{w_{ped}^2}$$



# Spreading: $\Gamma_{min}$ , Microturbulence (DW)

- What's the minimal pedestal fluctuation needed to broaden the SOL?
- The criterion:  $\lambda_e = \lambda_{HD}$ , or equivalently  $\tilde{v} = v_D$  when  $\tau = \tau_{\parallel}$ . ( $\lambda_e = \tau e^{0.5}$ )

For small scale fluctuations:

$$\tau_c \omega_s = \frac{\rho}{w_{ped}}$$

Effect of shear is not strong

1. Balance Linear Damping:

$$\Gamma_0 = |\gamma| \lambda_{HD}^3 \tau_{\parallel}^{-2}$$

Balancing with the estimation in the pedestal

$$\bullet \frac{e\delta\phi}{T_e} \sim \frac{|\delta v|}{c_s} \sim \left(\frac{3L_e}{aL_n}\right)^{0.25} q^{-0.25} (\rho/R)^{0.5}$$

2. Balance Nonlinear Damping:

$$\Gamma_0 = \alpha^3 \lambda_{HD}^9$$

Balancing with the estimation in the pedestal

$$\bullet \frac{e\delta\phi}{T_e} \sim \frac{|\delta v|}{c_s} \sim \left(\frac{L_e}{aL_n}\right)^{0.25} q^{1.5} (\rho/R)^{0.75}$$

THE Question:

Is the turbulence level in pedestal to broaden the layer compatible with good confinement?

→  $e\delta\phi/T_e$  small



# Spreading: $\Gamma_{min}$ , MHD (Ballooning)

- For Ballooning:  $\omega_s \tau_c = \sqrt{\beta_t} q \rho R / \left( w_{ped}^2 \sqrt{\frac{L_{pc}}{L_p} - 1} \right)$

Weak Shear Limit:

1. Balance Linear Damping:

- $\Gamma_0 \sim |\gamma| \lambda_{HD} v_D^2$
- $\frac{L_{pc}}{L_p} - 1 \sim (q\rho)^{4/3} \frac{R^{2/3} L_p^{8/3}}{L_p^2 \Delta_r^{8/3}} \beta_t$

2. Balance Nonlinear Damping:

- $\Gamma_0 \sim \alpha^3 \lambda_{HD}^9$
- $\frac{L_{pc}}{L_p} - 1 \sim \frac{\rho^2 q^6 L_p^{8/3}}{L_p^2 \Delta_r^{8/3}} \beta_t$

Strong Shear Limit:

1. Balance Linear Damping:

- $\Gamma_0 \sim |\gamma| \lambda_{HD} v_D^2$
- $\left( \frac{L_{pc}}{L_p} - 1 \right) \sim (q\rho)^{14/9} \frac{R^{10/9}}{L_p^{8/3}} \left( \frac{L_p}{\Delta_r} \right)^{16/9} \beta_t$

2. Balance Nonlinear Damping:

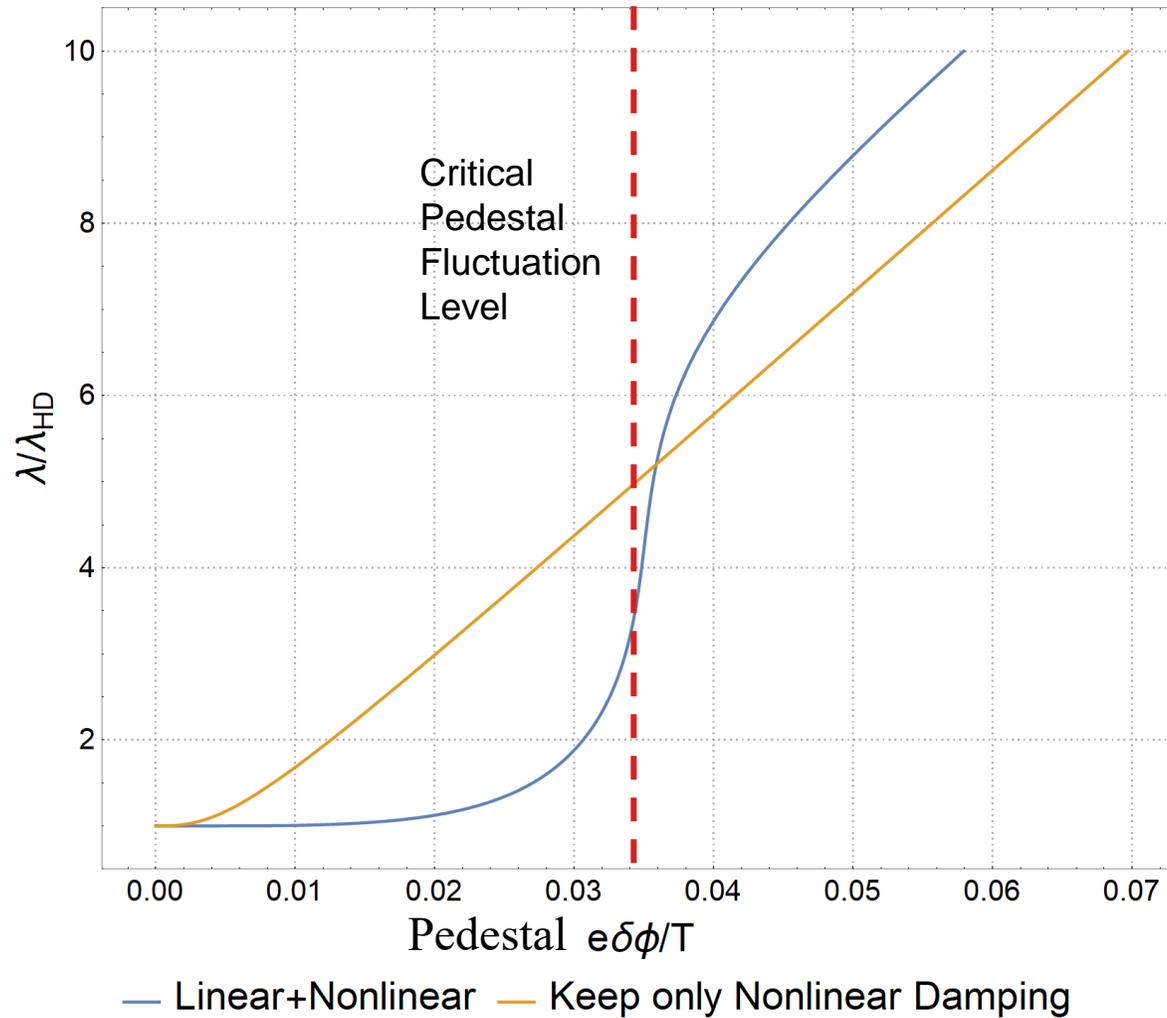
- $\Gamma_0 \sim \alpha^3 \lambda_{HD}^9$
- $\left( \frac{L_{pc}}{L_p} - 1 \right) \sim \frac{\rho^2 q^{14/3} R^{2/3}}{L_p^{8/3}} \left( \frac{L_p}{\Delta_r} \right)^{16/9} \beta_t$

$L_{pc}/L_p \sim 1 + \epsilon$ , weakly unstable  $\rightarrow$  Grassy ELM



# SOL Layer Width – Unified Estimation

- $\lambda_e = \lambda = \sqrt{\lambda_{HD}^2 + \tau_{\parallel}^2 e}$
- $\Gamma_e = \frac{(\sqrt{\beta/\lambda} - 3/\lambda^2)e\lambda}{+\sigma e^{1+\kappa}\lambda}$
- $\sigma = 0.6, \kappa = 0.5$
- The fluctuation level is converted from intensity flux using DW estimation
- Effective critical fluctuation level is required.



Maybe not so bad but soft pedestal



# Conclusions

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- SOL is linearly stable in H mode due to large  $E \times B$  shear and sheath resistivity
- Turbulent spreading from the pedestal can broaden the layer and should be considered
- SOL width is related to intensity flux across the separatrix which is in turn determined by pedestal parameters
- Intensity flux balances linear and nonlinear damping in the SOL
- There exist a minimal intensity flux for spreading such that  $\lambda > \lambda_{HD}$
- Identifies the key question: Can turbulent pedestal broaden  $\lambda$  while maintaining adequate confinement?)
  - Point to turbulent pedestal states



# For Experimentalists

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- Direct Measurement of Turbulence Spreading at Separatrix (Ting Wu)
- Correlation of Spreading, Edge Intensity Levels to SOL Width
  - Special Attention to Heat Load Width in Turbulent Pedestal States
- Connection between Spreading and Blob Generation
- Is blob simply the end state of turbulent spreading event?



# Back transition and HDL

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- Future research:
  - HDL: Strong layer broadening weakens shear stabilization and makes SOL interchange unstable.
  - Does SOL turbulence then invade pedestal, cause H→L, defining HDL?
    - From Dog→Tail to Tail→Dog
  - Two levels: onset and invasion, Gap?
- $\Gamma_{max}$  broadens the SOL width and makes SOL linearly marginally stable:  $\gamma(\lambda_m) = 0$ 
  - $\lambda_m = \beta^{-1/3} 3^{2/3}, \Gamma_{max} = \sigma e^{1+\kappa} \lambda_e$

