

How does negative triangularity mitigate ITG turbulence and transport?

[Under review NF 2024]

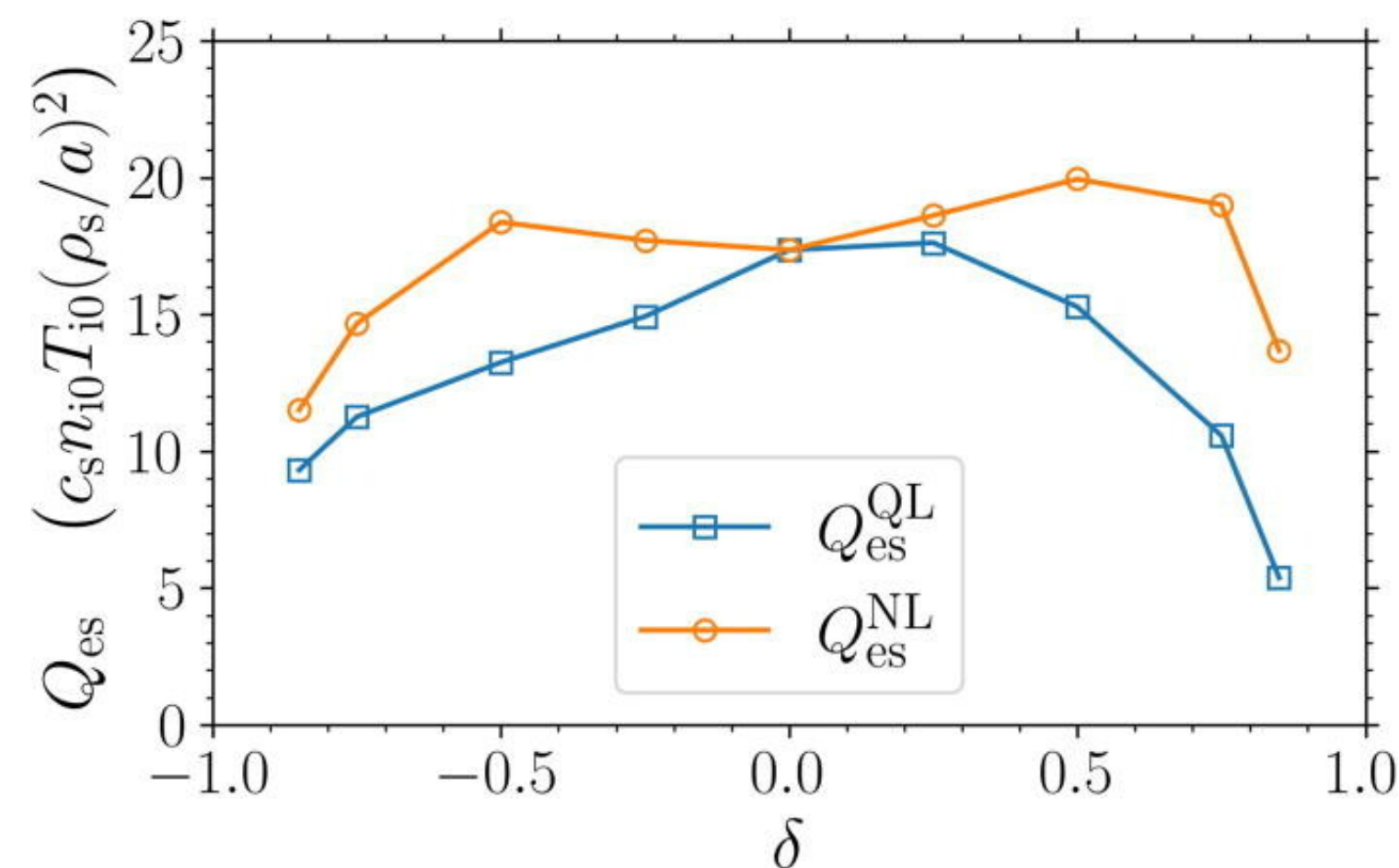
Rameswar Singh, P H Diamond and A Marinoni
UCSD

66th APS DPP, Atlanta, October 11, 2024

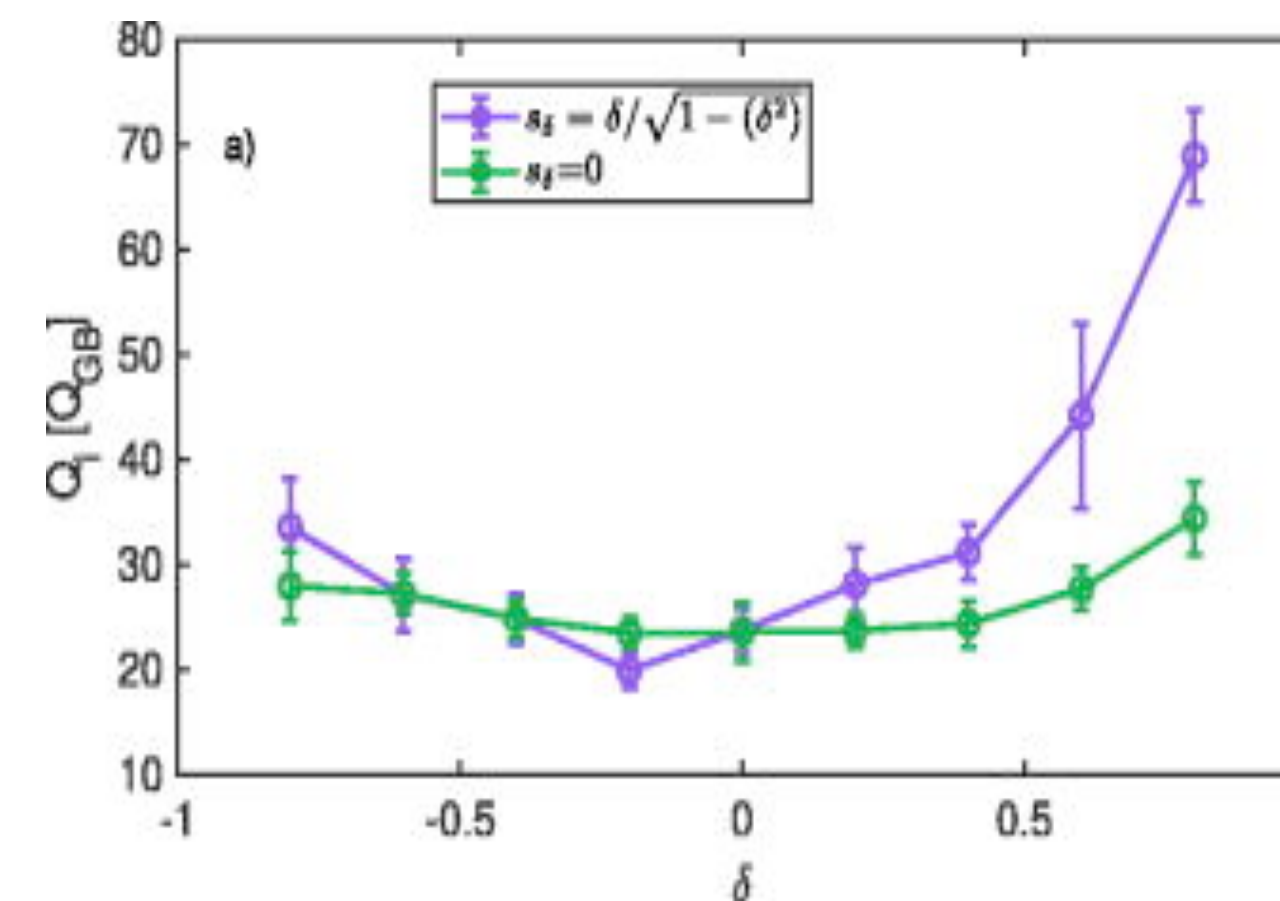
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Motivation

- Improved confinement in NT over PT tokamak experiments is now well established. [Y Camenen+ 2007, M Fontana+2018, M Austin+ 2019, A Marinoni+ 2019, S Coda+2022,...]
- Theoretical understanding lacking! TEM/ITG stabilization often invoked to explain improved confinement in NT.
 - TEM stabilization by precession drift reduction. [A Marinoni+ 2009]
 - ITG turbulence and transport for NT remains poorly understood.
- Previous simulations lacked insights on physical mechanism behind the beneficial effects of NT on ITG . Sometimes, not even general agreement on basic trends with δ !



[J M Duff+ 2022]



[G Merlo+ 2023]

Questions remain...

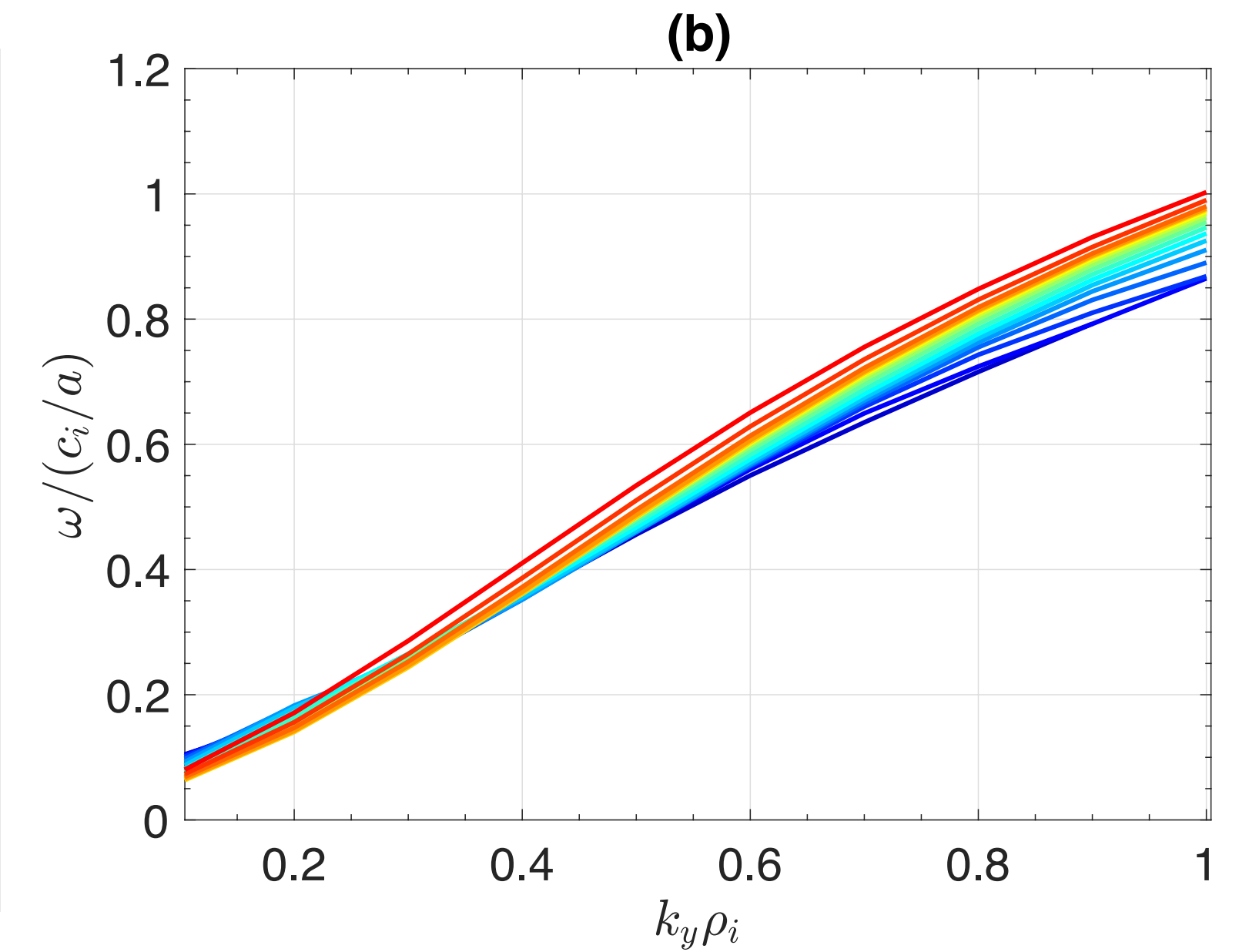
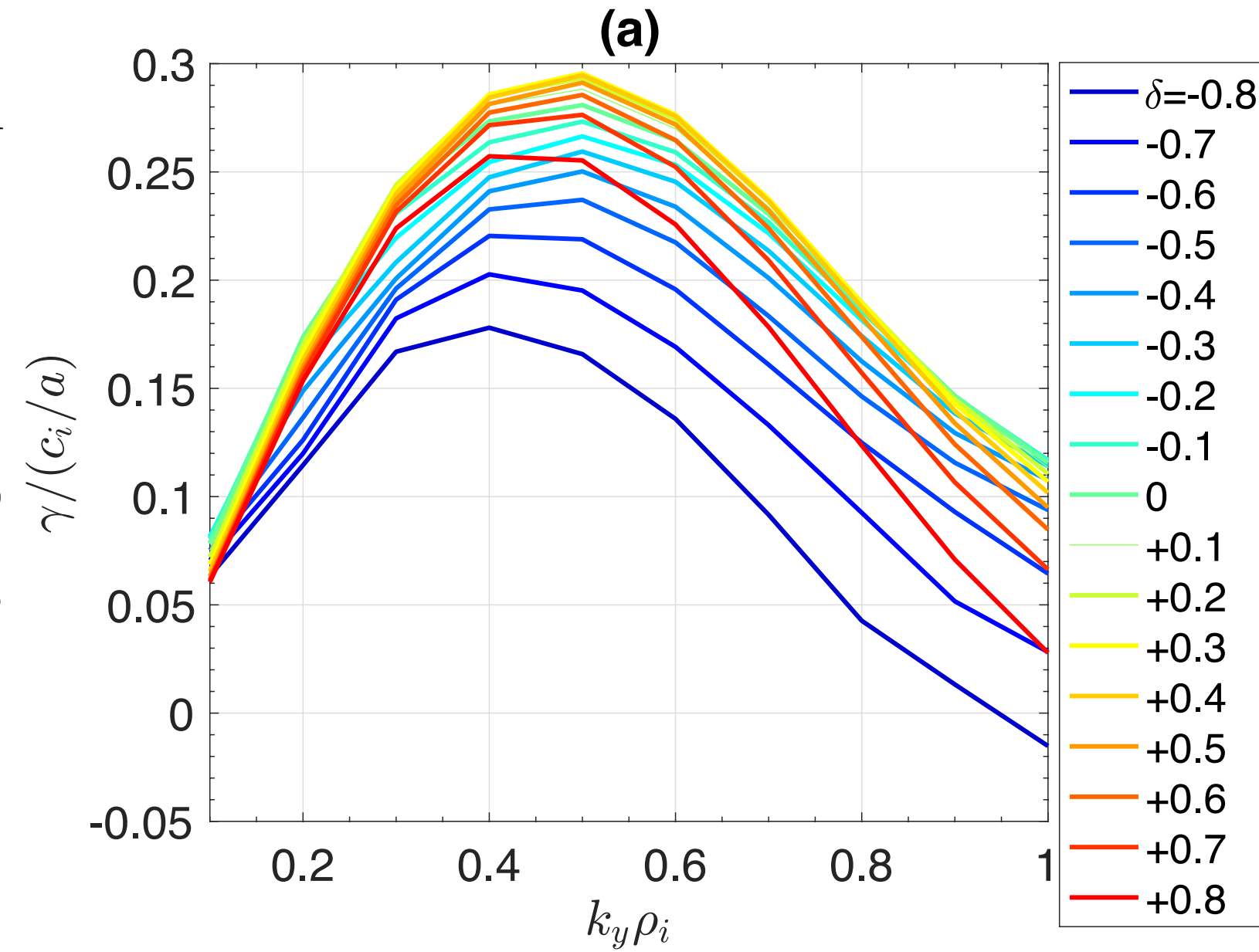
- What causes the reduced linear growth rate for NT?
- What explains the δ -trend of heat flux?
 - Relative role of fluctuations amplitude and cross-phase in determining the heat flux for NT?
 - Saturation by zonal flows well known in GK simulations [[Z Lin+ 1998,1999,...others](#)]. What happens to self-generated zonal flow shear for NT?

Simulation set up

- **Disclaimer:** This is a physics study, not an experimental validation exercise.
- GENE flux tube simulations of **collisionless ITG** turbulence with adiabatic electrons. **Profiles fixed, triangularity varied.**
- **Shaping parameters:** aspect ratio $a/R = 1/3$, safety factor $q = 2$, magnetic shear $\hat{s} = 1$, **triangularity** $\delta = [\text{varied}]$, triangularity gradient $S_\delta = \frac{r \frac{\partial \delta}{\partial r}}{\sqrt{(1 - \delta^2)}} = \frac{\delta}{\sqrt{(1 - \delta^2)}}$, elongation $\kappa = 1$, elongation gradient $S_\kappa = \frac{r \frac{\partial \kappa}{\partial r}}{\kappa} = 0$, squareness $\zeta = 0$, squareness gradient $S_\zeta = r \frac{\partial \zeta}{\partial r} = 0$, MHD alpha parameter $\alpha_{MHD} = -q^2 R \frac{d\beta}{dr} = 0$, Shafranov shift gradient $R'_0 = 0$. (Standard GA + shaping)
- **Resolutions:** $n_x = 257$, $n_{k_y} = 48$, $n_z = 64$, $n_{v_{\parallel}} = 48$, $n_\mu = 8$, $L_{v_{\parallel}} = 3$, $L_\mu = 9$, $L_x = [120 - 140]\rho_i$, $k_{y,min}\rho_i = 0.05$, hyp_z=2, hyp_v=0.2
- **Gradients:** $a/L_n = 1$, $a/L_T = 4$ **[fixed]**
- **Collisionless:** => no frictional damping of ZF.
- **No neoclassical transport.**

Linear growth rates are reduced for NT

- Growth rates are lower for NT than for PT.
- **Why?**
- **Linear stability linked to eigenmode averaged quantities**
 $\langle \omega_{Dy} \rangle, \langle k_{\perp}^2 \rangle, \langle k_{\parallel}^2 \rangle$.



Eigenmode averaged magnetic drift frequency is reduced for NT

- Eigenmode averaged drift frequency:

$$\langle \omega_{Dy} \rangle = \frac{\int d\theta JB |\phi|^2 \omega_{Dy}}{\int d\theta JB |\phi|^2}, \text{ where}$$

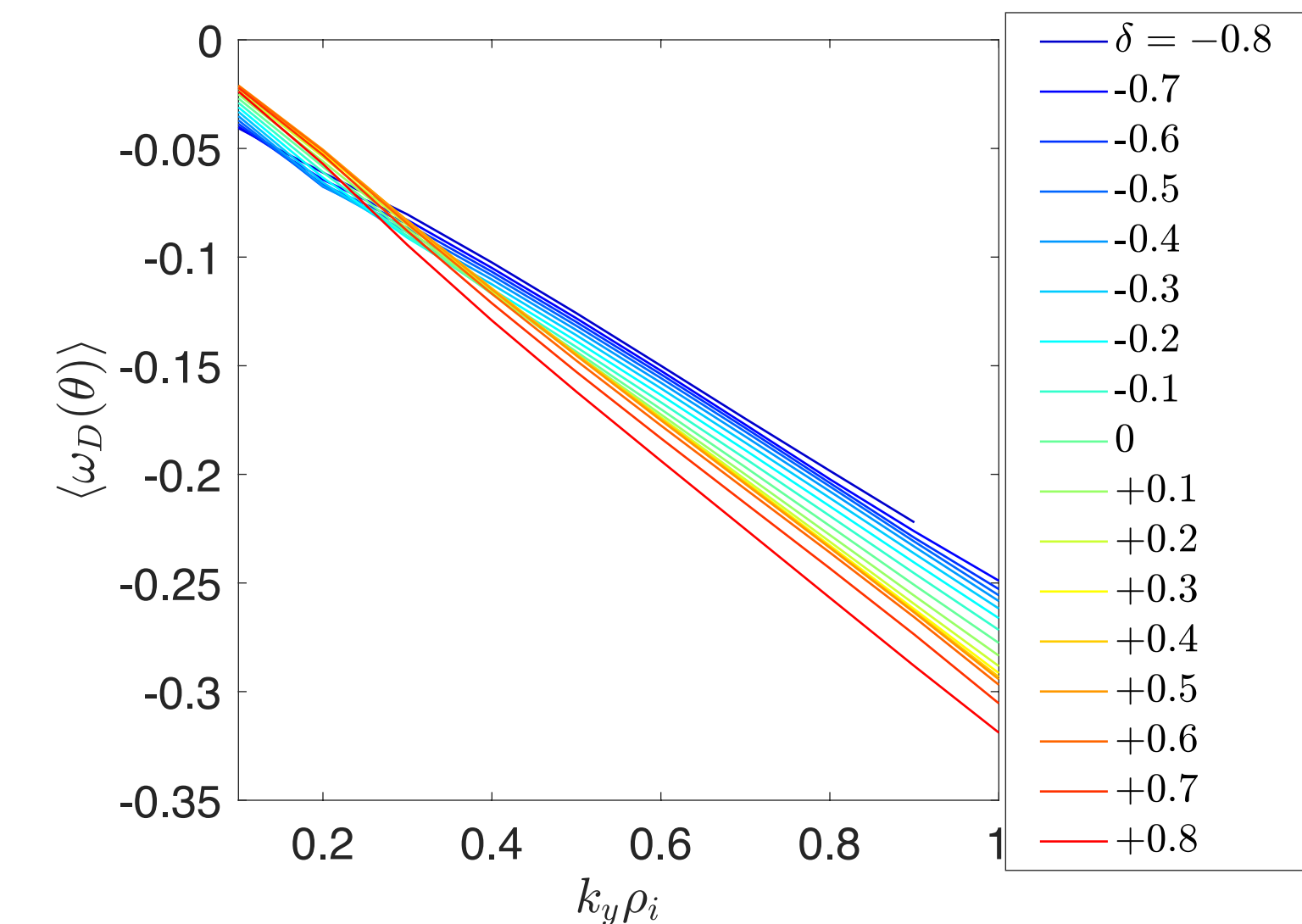
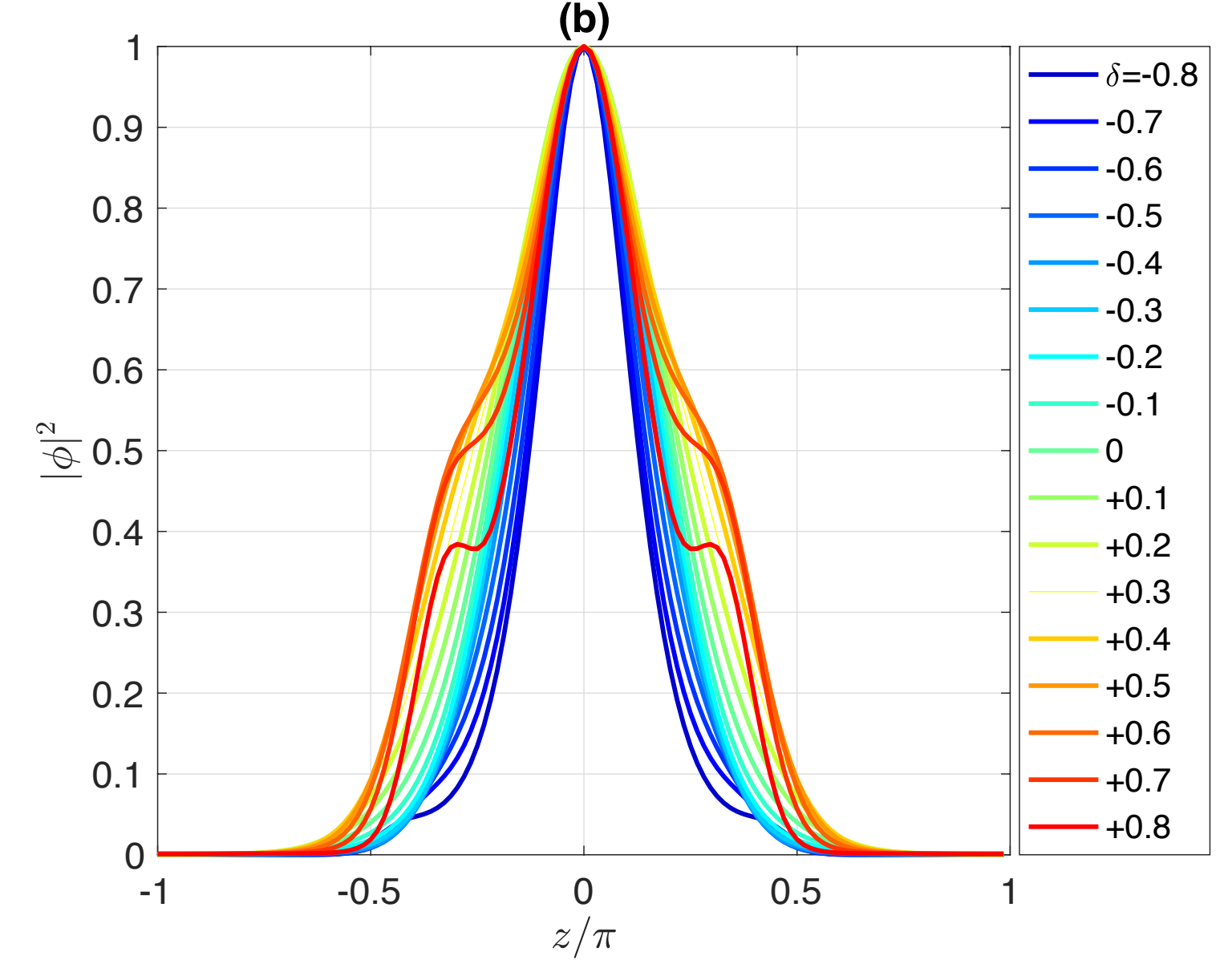
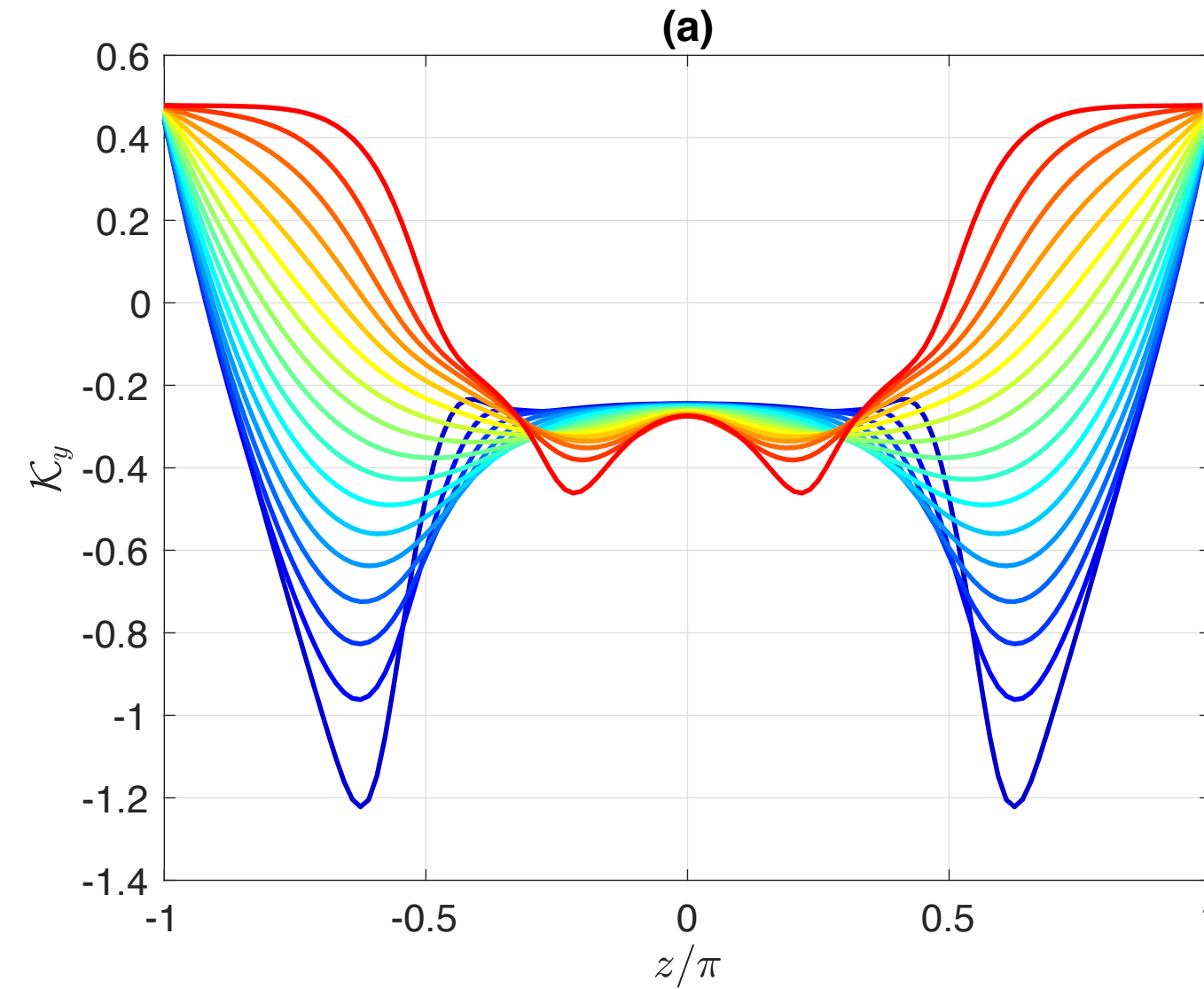
- $\omega_{Dy} = k_y \frac{v_{\parallel}^2 + v_{\perp}^2/2}{\Omega} \mathcal{K}_y$ is binormal magnetic drift frequency

- $\mathcal{K}_y = \frac{1}{B} \vec{b} \times \vec{\nabla} B \cdot \vec{\nabla} y$ is binormal curvature

- \mathcal{K}_y less negative for at $z = 0$ NT.
- Broader negative \mathcal{K}_y region for NT.
- But thinner eigenmode width for NT

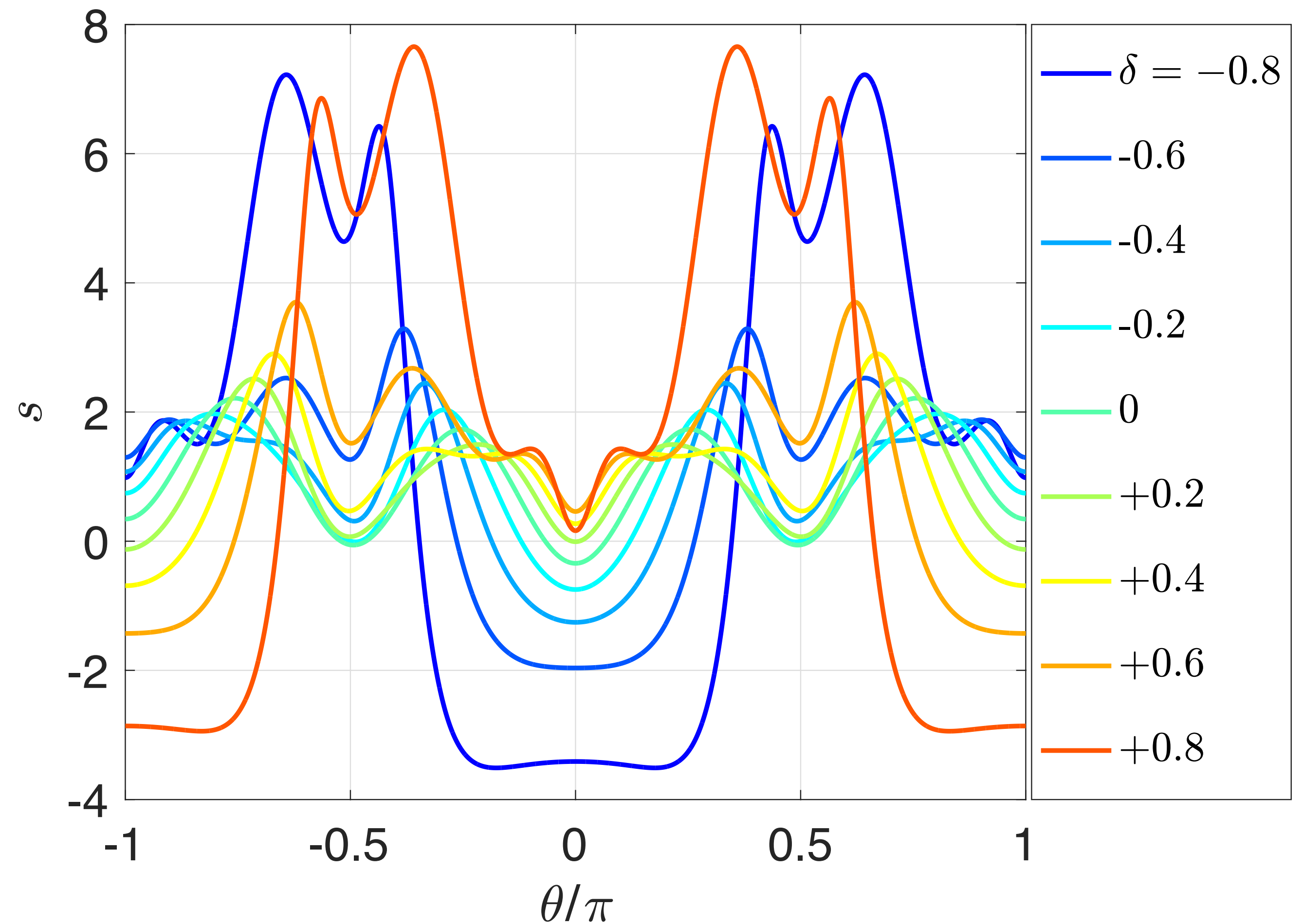
➔ Less negative $\langle \omega_{Dy} \rangle$ for NT. →

➔ weaker effective curvature drive for NT, due to reduced sampling of the bad curvature regions resulting from a narrow eigenmode structure in NT.

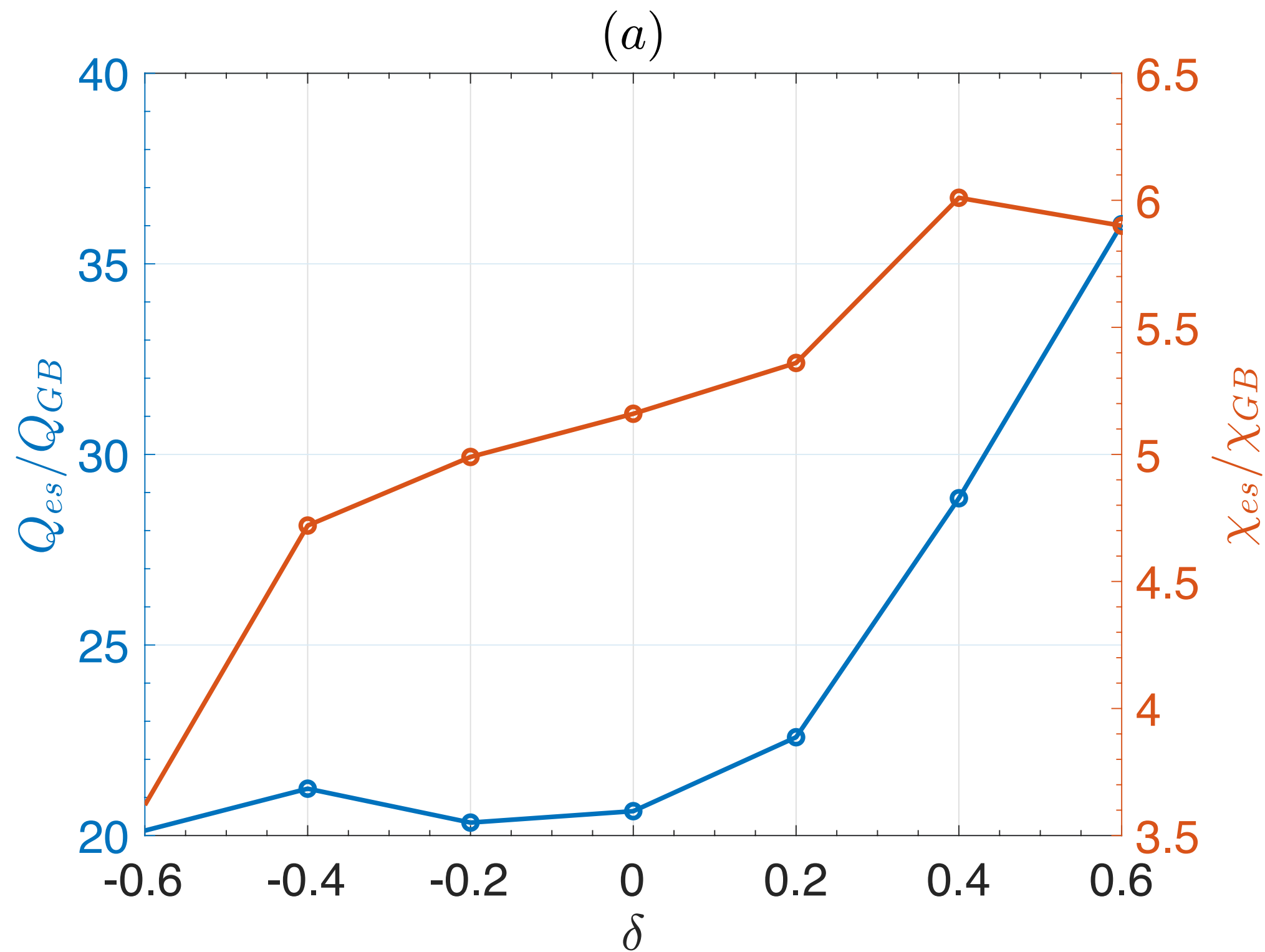


Local magnetic shear \tilde{s}

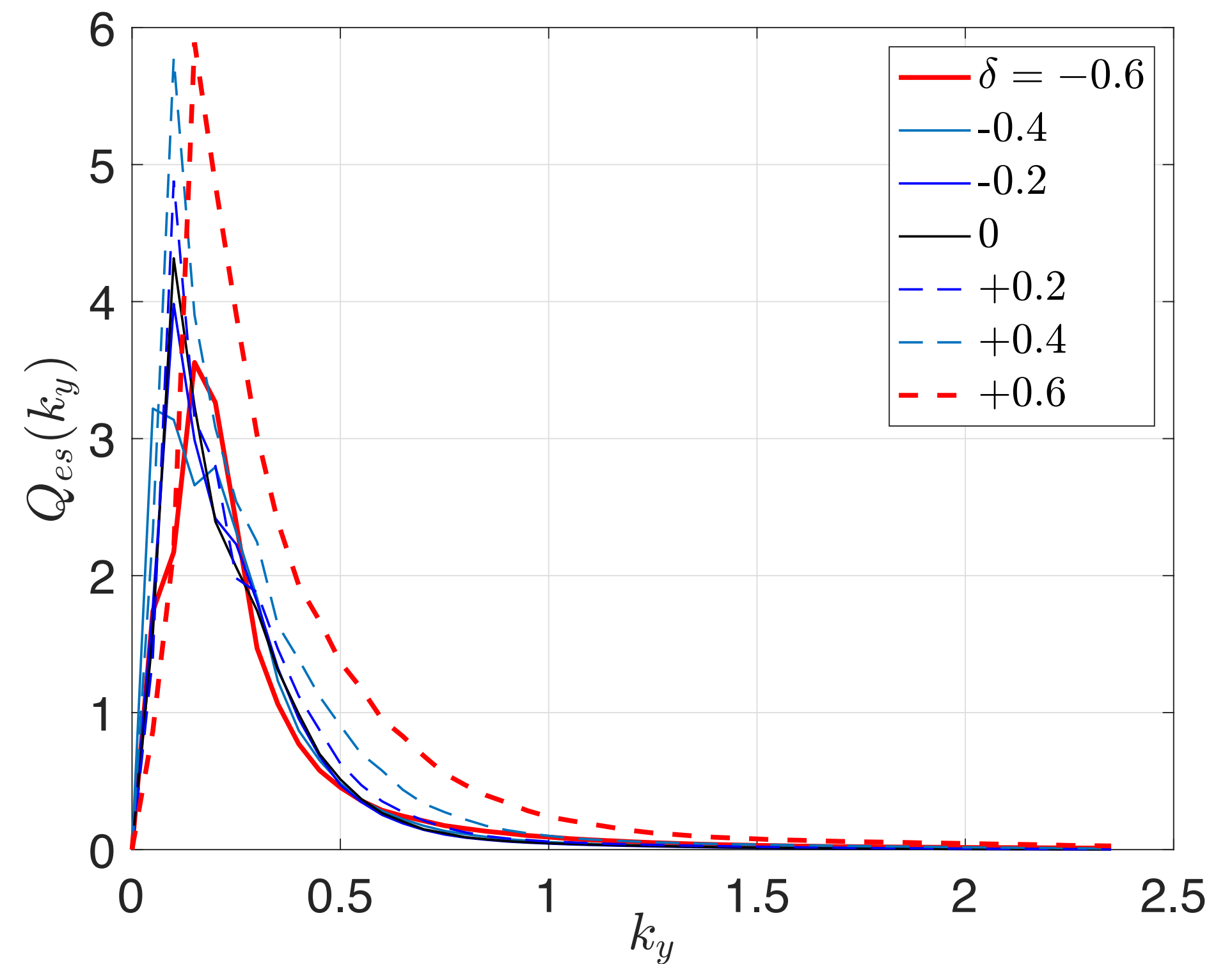
- $\tilde{s} = \frac{r}{\nu} \frac{\partial \nu}{\partial r}$, where $\nu = IJ/R^2$ is the local safety factor.
- More and more negative \tilde{s} in the bad curvature region and the poloidal extent of the $\tilde{s} < 0$ region expands for stronger NT shapes
- **→easier to twist eddies towards the good curvature side as you move along the field line →better stability for NT!**



Nonlinear Heat flux vs Triangularity



- Turbulent heat diffusivity lower for NT than for PT.
- High k_y contributions (RHS of the spectral peak) depleted more for NT.



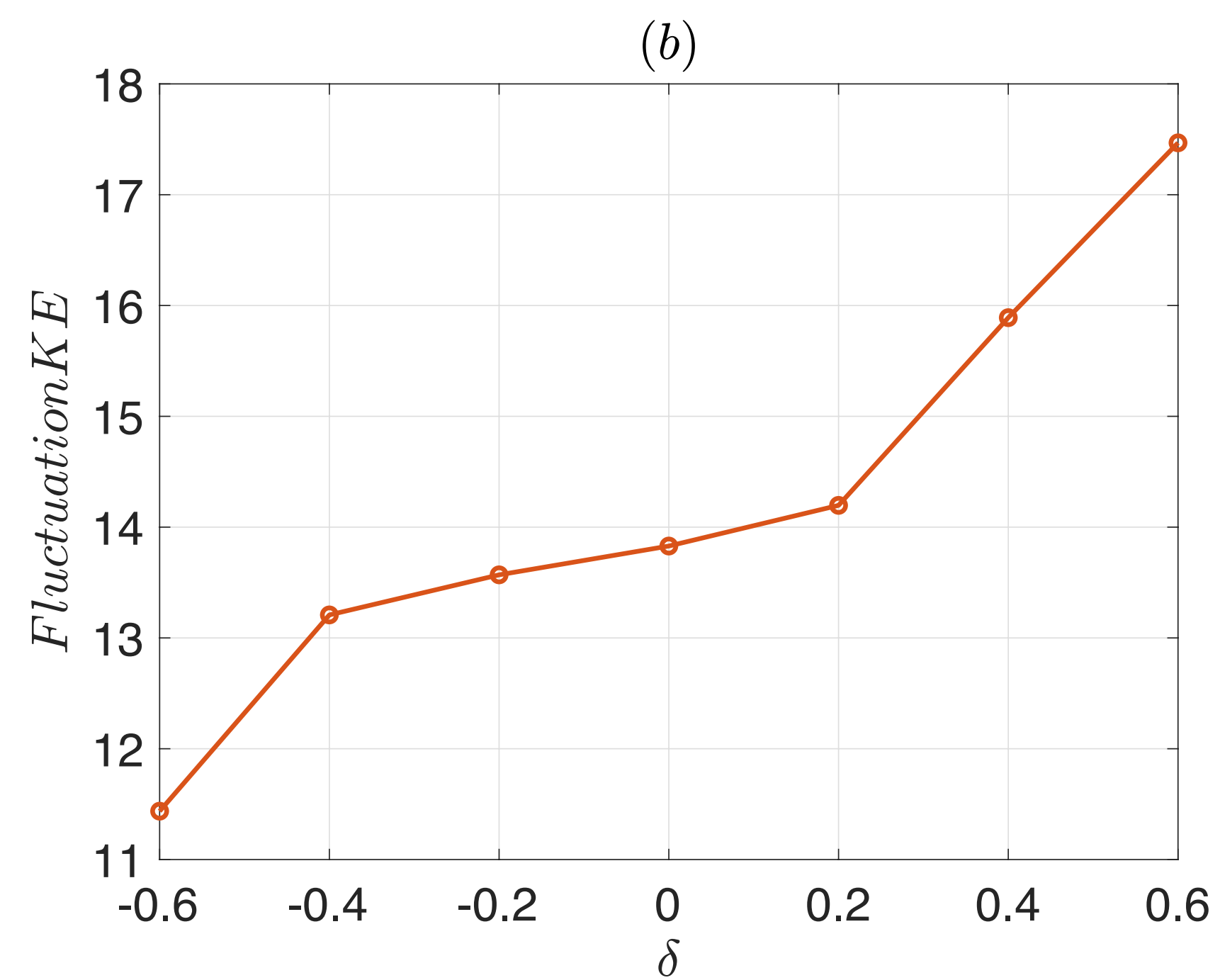
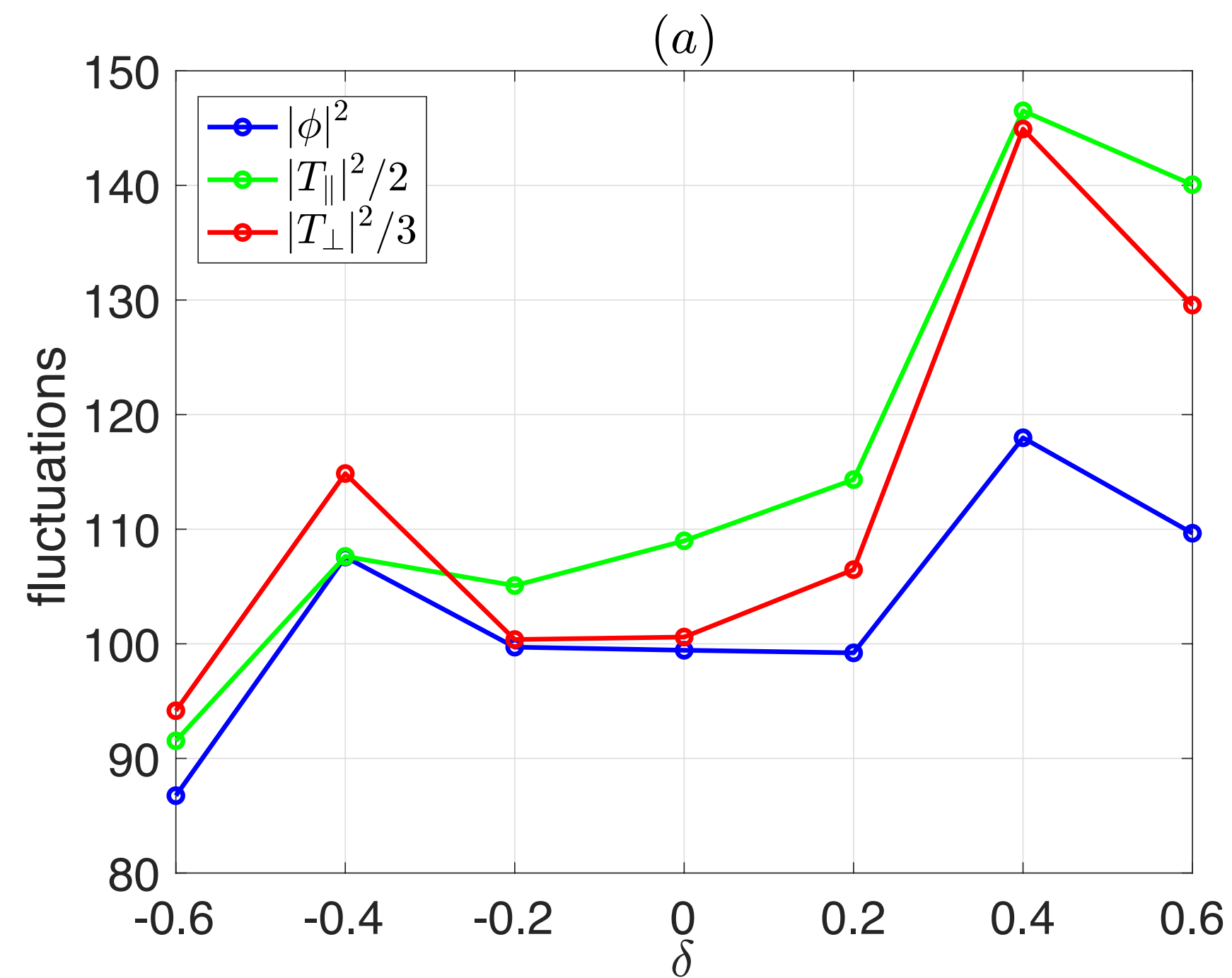
• Heat flux $Q_i = \left\langle \sum_{\vec{k}} -k_y |T_k| |\phi_k| \sin(\theta_T - \theta_\phi) \right\rangle$

Amplitudes Cross-phase

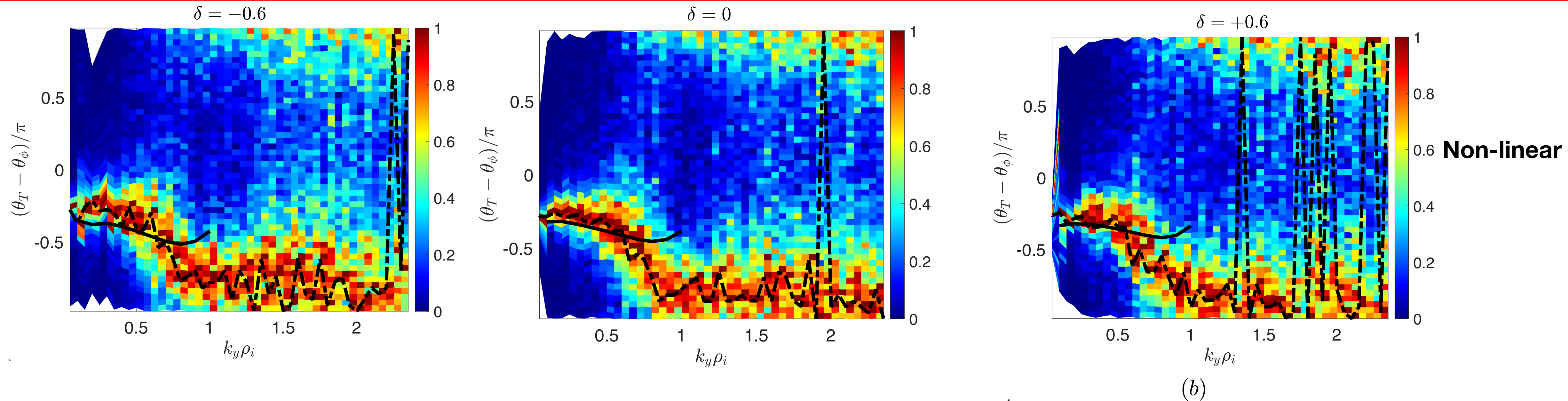
Saturated fluctuation intensity vs Triangularity

- Fluctuation intensities are lower for NT than for PT.

- Fluctuation kinetic energy: $FKE = \left\langle \sum_{k_x, k_y} [1 - \Gamma_{0i}(k_{\perp}^2 \rho_i^2)] \left| \frac{e\delta\phi_k}{T_i \rho^{\star}} \right|^2 \right\rangle$ is lower for NT!

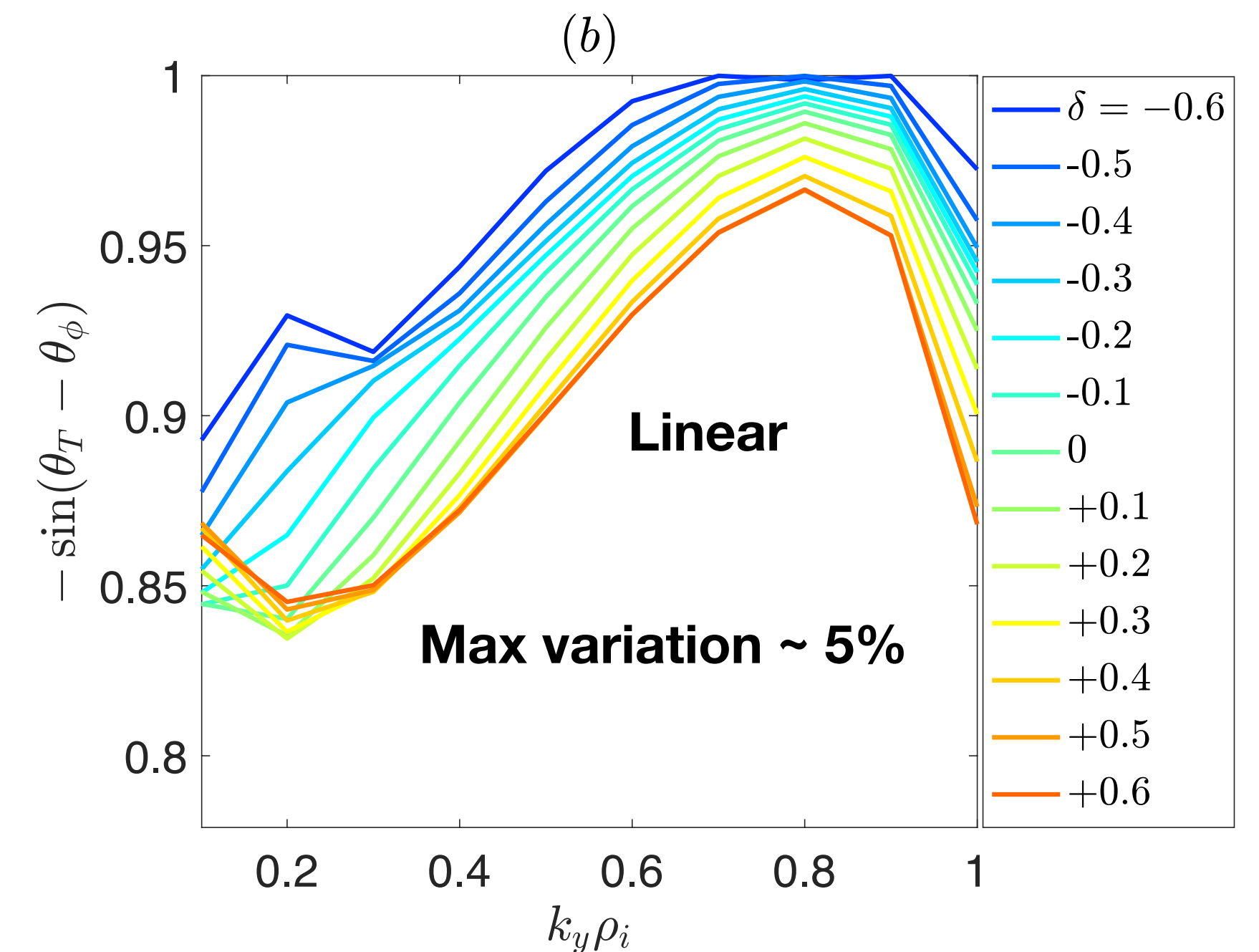


Transport cross-phase spectra vs Triangularity

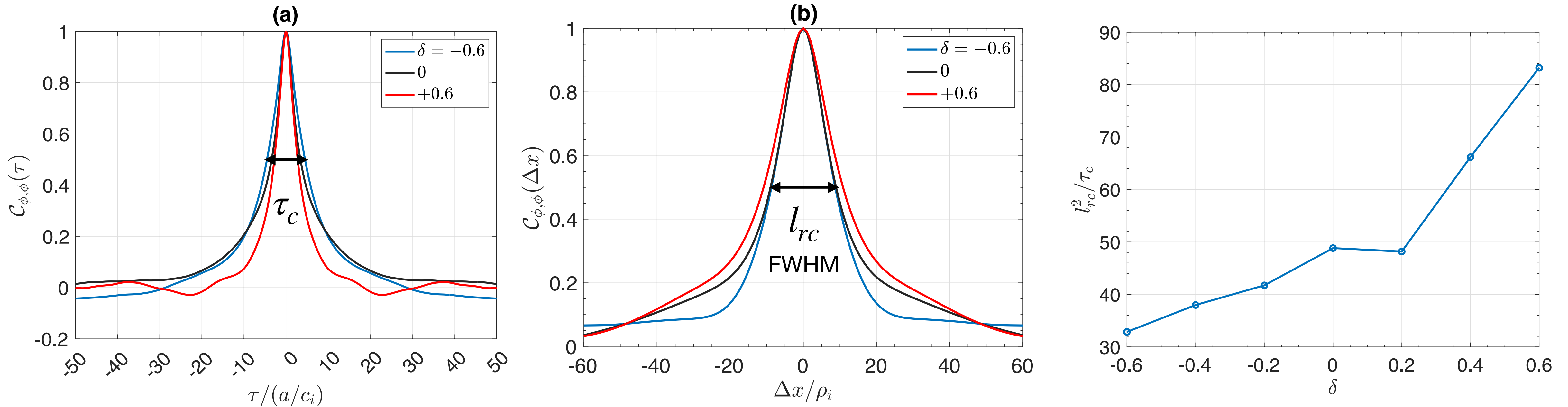


- Cross phases between temperature and potential fluctuations $(\theta_T - \theta_\phi)$ are weakly sensitive to δ .

➡ Transport reduction for NT is pre-dominantly due to reduction of fluctuation amplitudes.

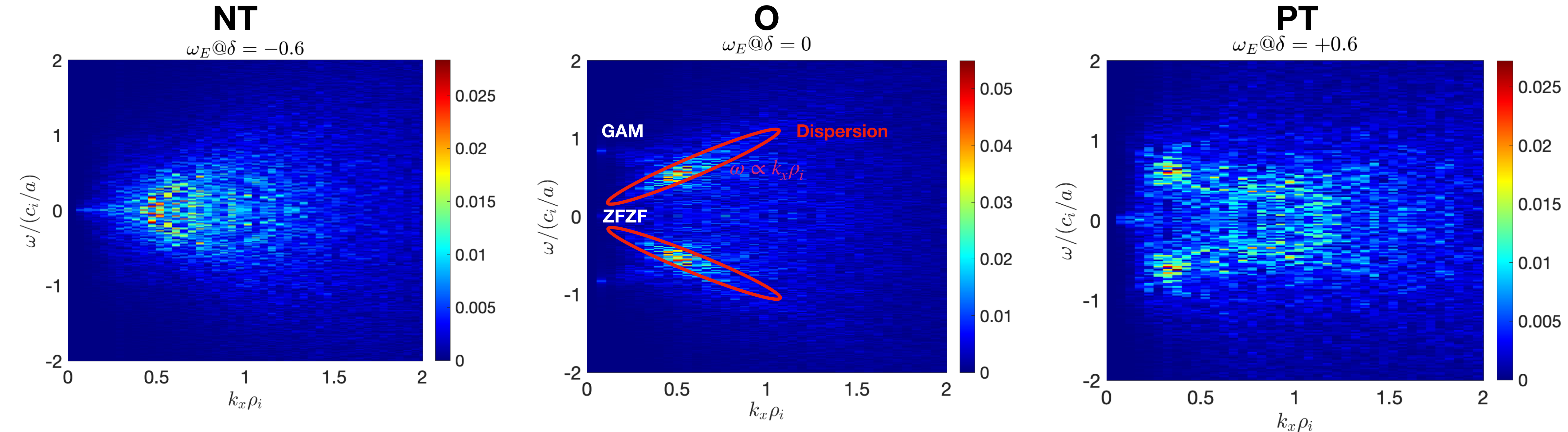


Fluctuations auto-correlation and random walk diffusivity



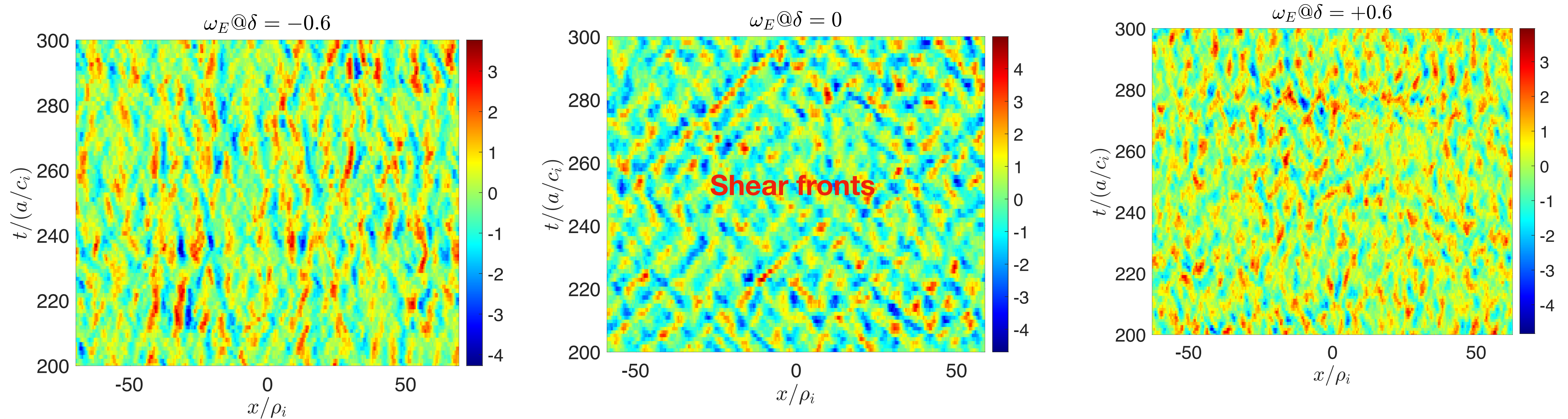
- Auto-correlation time higher for NT: $\tau_c(NT) > \tau_c(PT)$
 - Radial auto-correlation length lower for NT: $l_{rc}(NT) < l_{rc}(PT)$ [Consistent with TCW experiment: M Fontana+ 2018]
- ➔ Random walk diffusivity $\frac{l_{rc}^2}{\tau_c}$ lower for NT.

Zonal ExB shearing rates: $\omega - k$ spectra



- Shearing spectra are highly sensitive to δ .
 - No dispersive effect for $\delta = -0.6$
 - **Clear dispersive effects for $\delta = 0 \rightarrow$ propagating zonal flows (New branch)**
 - Weak dispersion for $\delta = +0.6$
- The spectra roll over at \sim GAM frequency

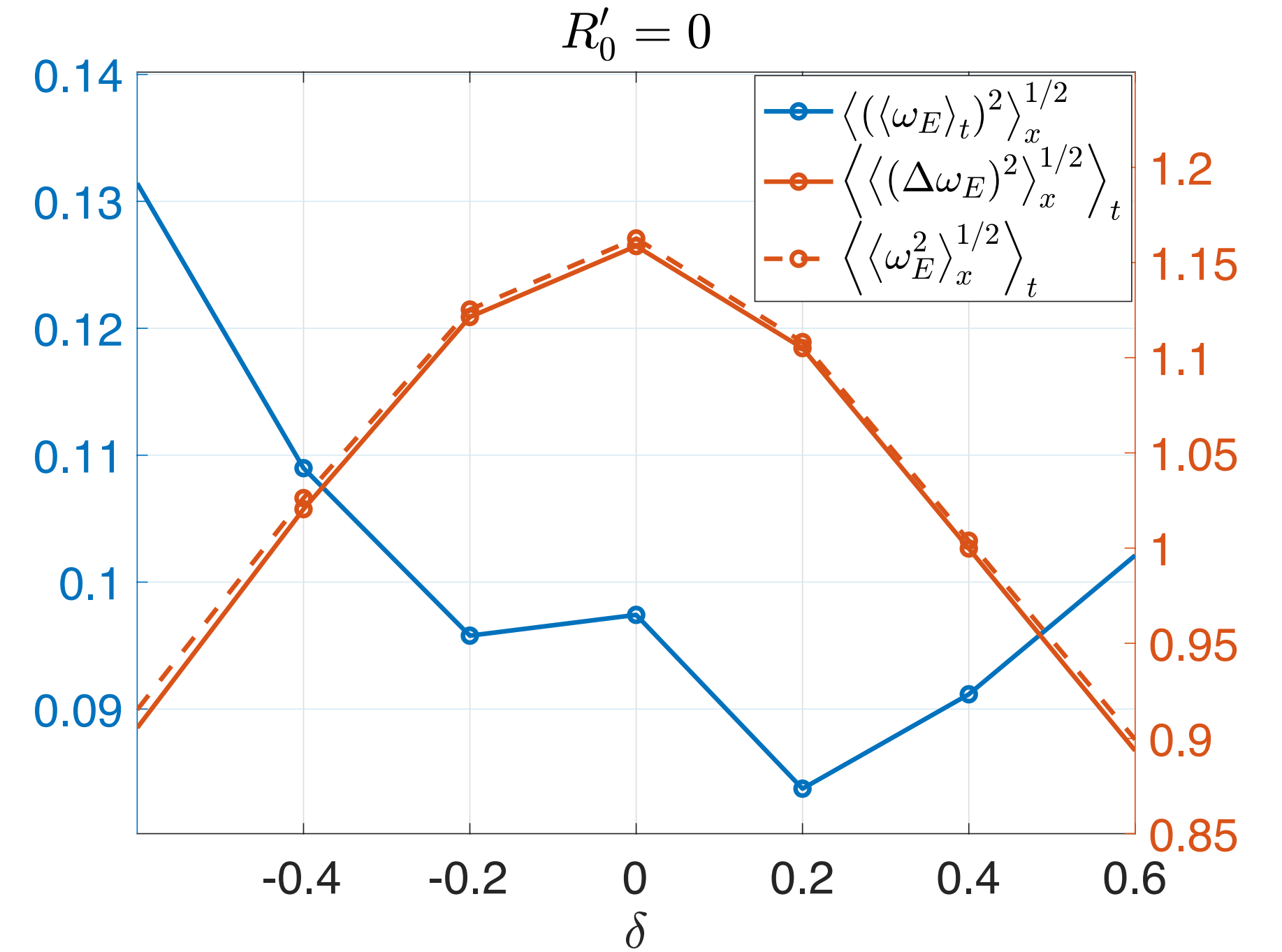
Zonal ExB shearing rates: spatiotemporal features



- Spatiotemporal patterns are highly sensitive to δ .
 - **Spatiotemporal shearing pattern more coherent for NT than for PT.**
 - Propagating shearing fronts \rightarrow dispersive feature for $\delta = 0$! Front speed $\sim 2.25\rho_\star v_{th}$.
- **More coherent spatiotemporal shearing pattern for NT \rightarrow Stronger mean shearing effect for NT.**

RMS Zonal ExB shearing rates at saturated state

- **Zero-frequency RMS shearing rate higher for NT than for PT.**
- Total RMS shearing rate and finite frequency RMS shearing rate decreases with increasing $|\delta|$.



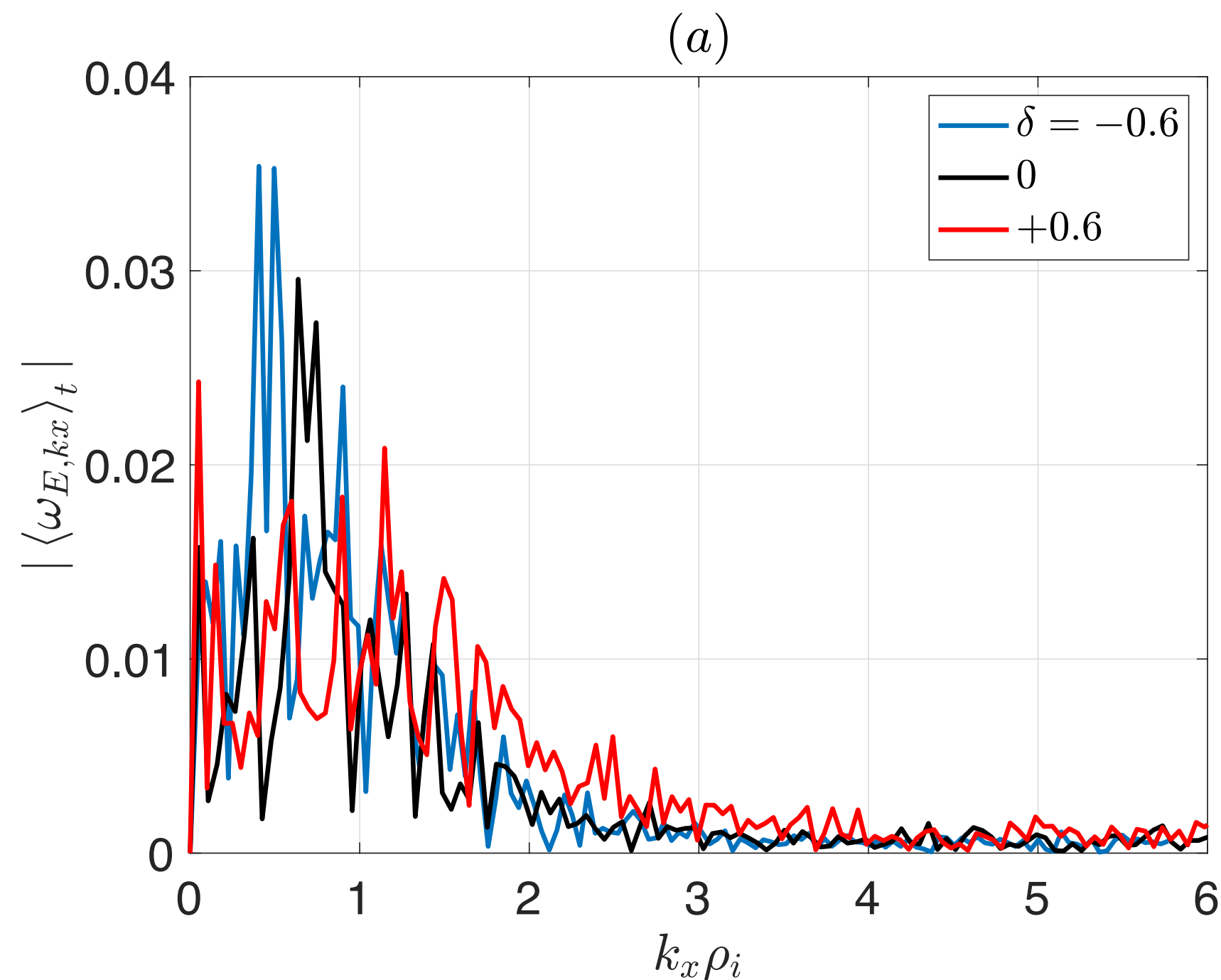
* Time averaged or zero-frequency RMS shearing rate: $\langle \langle (\omega_E)_t \rangle_x^2 \rangle_t^{1/2} = \left[\frac{1}{L_x} \int dx \langle \omega_E(x, t) \rangle_t^2 \right]^{1/2}$, where $\langle \omega_E(x, t) \rangle_t = \frac{1}{T} \int dt \omega_E(x, t)$

* Total RMS shearing rate: $\langle \langle \omega_E^2(x, t) \rangle_x \rangle_t^{1/2} = \left[\frac{1}{T} \int dt \frac{1}{L_x} \int dx \omega_E^2(x, t) \right]^{1/2}$

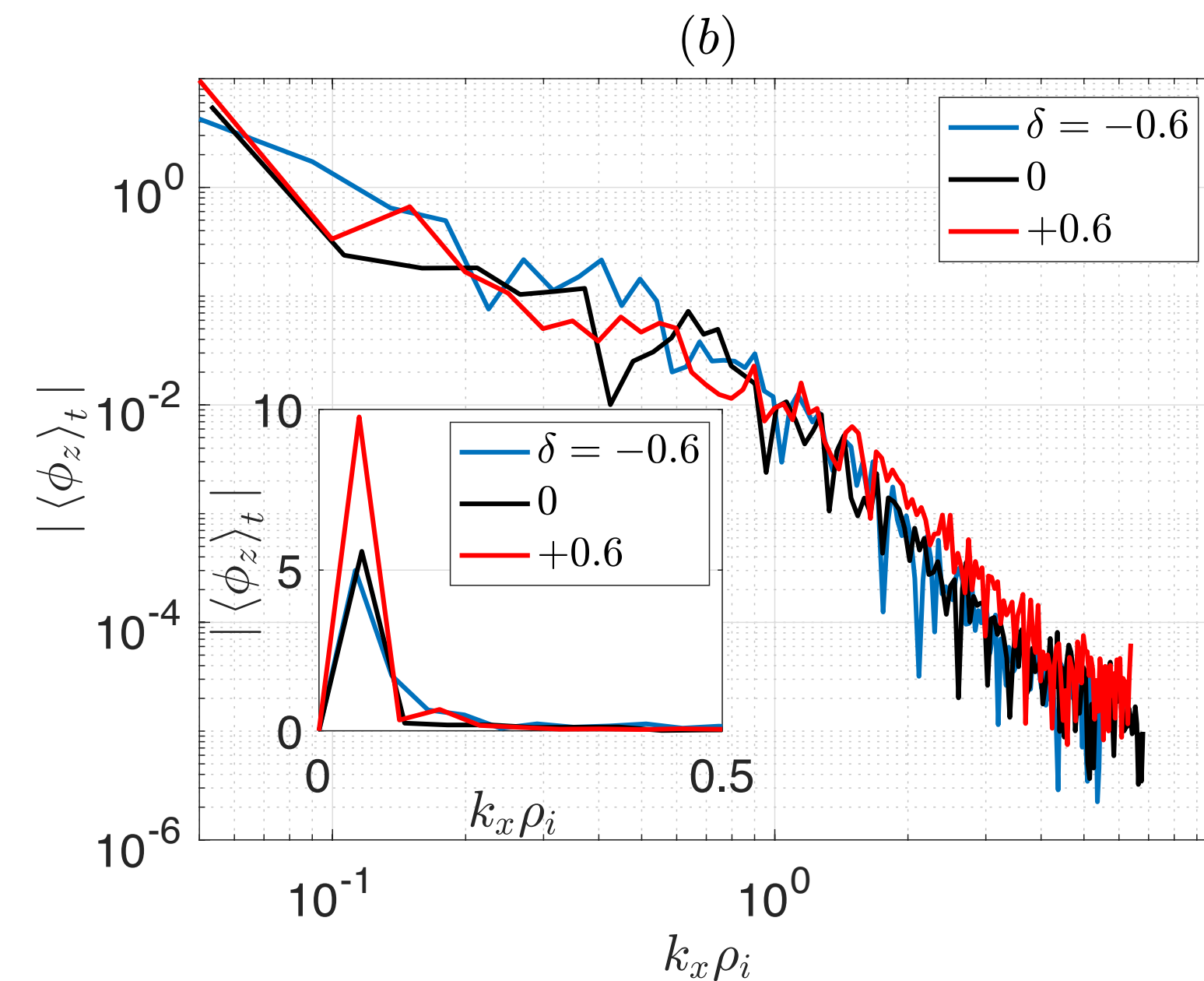
* Standard deviation of shearing rate: $\langle \langle (\Delta\omega_E)^2 \rangle_x^{1/2} \rangle_t = \left\langle \left\langle \left(\omega_E(x, t) - \langle \omega_E(x, t) \rangle_t \right)^2 \right\rangle_x^{1/2} \right\rangle_t$

RMS shearing rate depends on the detail of the shearing spectra at saturated state

- **Different δ -trend of zero-frequency shearing rate and zonal potential spectra.**
- Zonal shear peak at $k_x \rho_i \sim 0.5$ whereas zonal potential peak at $k_x \rho_i \sim 0.05$.
- **Shearing peak stronger while potential peak weaker for NT.**



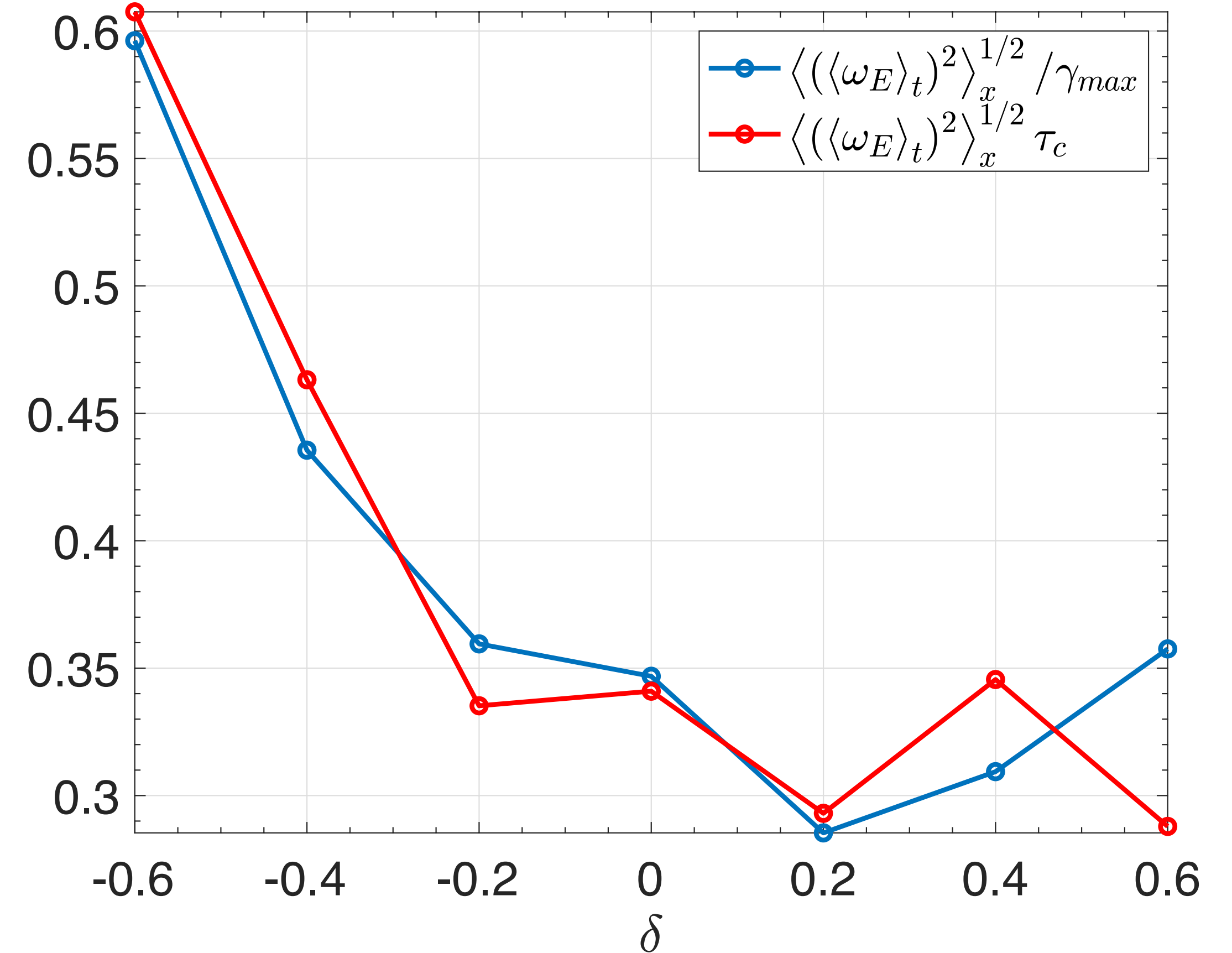
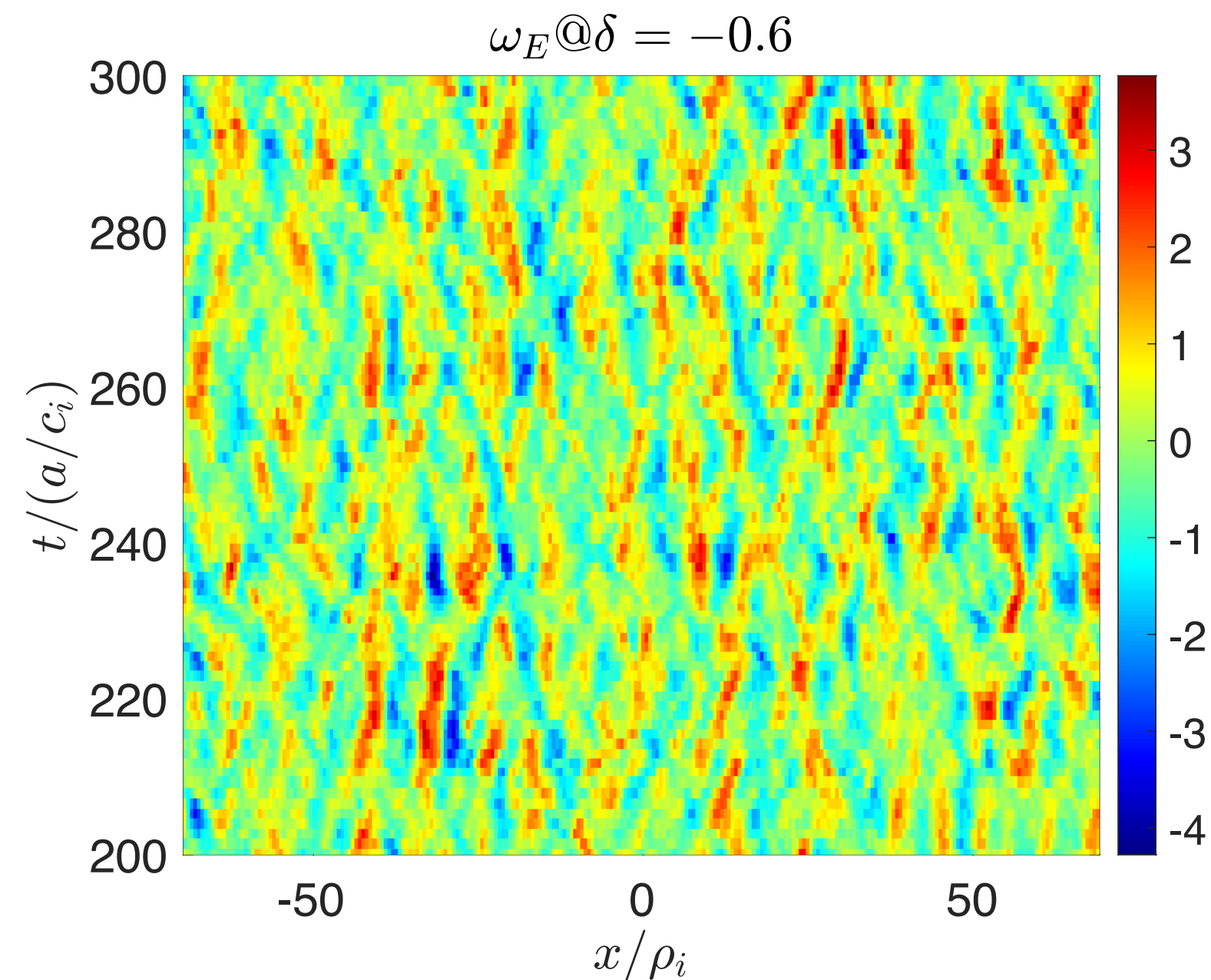
Shearing peaks stronger for NT than for PT.



Zonal potential peaks weaker for NT for PT. But zonal potential isn't the point.

Figure of Merit

- All analyses point at the dimensionless parameter $\omega_E \tau_c$ or ω_E / γ_{max} as *figure of merit*.
- $\omega_E \tau_c$ higher for NT than for PT. Nicely correlates with the δ -trend of heat diffusivity.



Summary

- Novel insights into how NT mitigates ITG turbulence and transport



$\omega_E \tau_c$ or ω_E / γ_{max} as *figure of merit*.

- Reduced linear growth rate for NT



Reduced eigenmode averaged magnetic drift frequency.

- Reduced heat flux for NT



Reduced radial correlation length and increased correlation time due to increased zero-frequency zonal ExB shearing rate.

- δ -trend of diffusivity



Predominantly determined by δ -trend of fluctuation amplitude. Cross-phase effect weak.

Future work

- Understanding why zero-frequency zonal shearing stronger for NT → requires analysis of Reynolds power $\frac{\partial \langle v_\theta \rangle}{\partial r} \langle \tilde{v}_r \tilde{v}_\theta \rangle$. More generally, gyrokinetic nonlinear entropy transfer analysis required. Collisionless zonal flow saturation dynamics?
- Analysis using experimental equilibria and profiles and using non-adiabatic electrons and finite collisionality exploiting both local and flux driven global simulations.

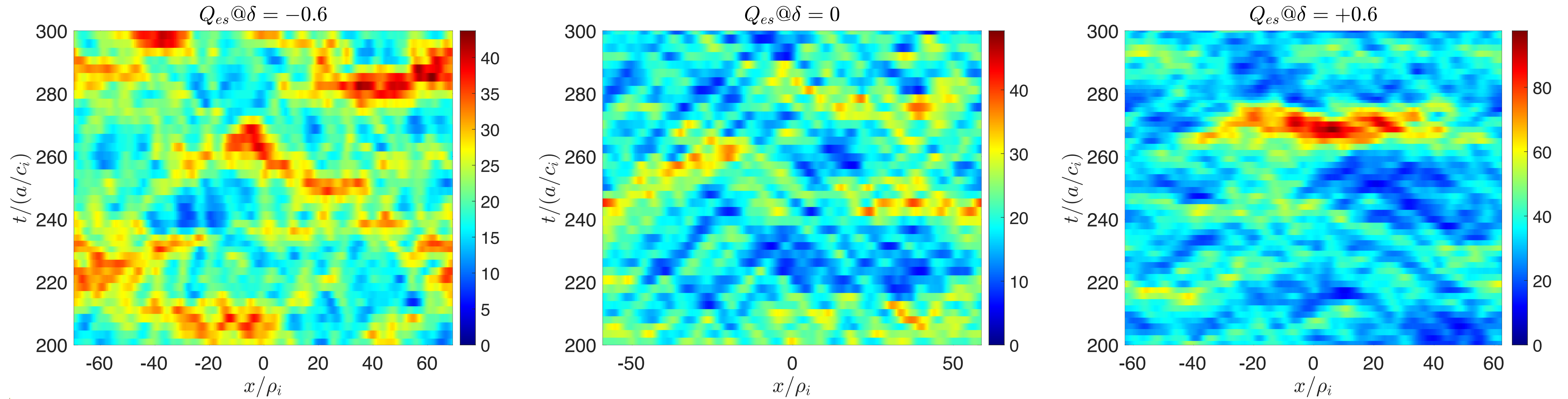
For experiments

- **Measure $\omega - k$ spectra of the zonal flow shear.** Identify finite frequency components? Spatio-temporal features of zonal shear, signatures of propagating zonal fronts \rightarrow BES velocimetry
- Study, identify different trends of zero-frequency zonal potential and zonal flow shear with δ .
- Bi-spectral analysis to identify how dominant interactions change with triangularity ?
- Frequency resolved Reynolds power $\frac{\partial \langle v_\theta \rangle}{\partial r} \langle \tilde{v}_r \tilde{v}_\theta \rangle$ vs triangularity to elucidate turbulence \rightarrow zonal flow energy coupling? \rightarrow BES velocimetry.
- Radial correlation length and auto-correlation time of fluctuations and zonal flows. **Calculate FOM $\omega_E \tau_c$ vs δ .**

Back-up slides

Heat flux avalanches

- Avalanches also seen in heat flux space time evolutions.



Temperature corrugations dynamics

(a) Zonal temperature spectrally anti-correlated with zonal potential $T_{z,k_x} \propto -\phi_{z,k_x}$. Consequently, zonal ExB shear ω_E is spatially anti-correlated with zonal temperature curvature $\nabla^2 T_z$.

(b) Zonal temperature corrugations are stronger for NT than for PT.

