

# Dynamics of **intrinsic axial flow** in a cylindrical experimental plasma

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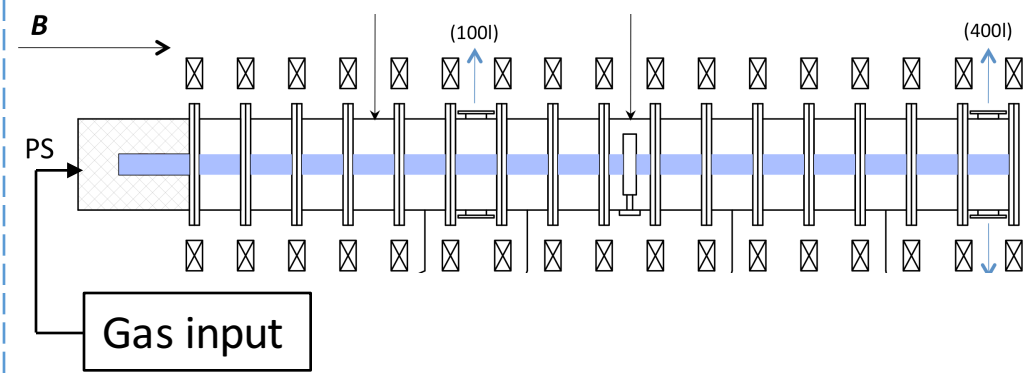
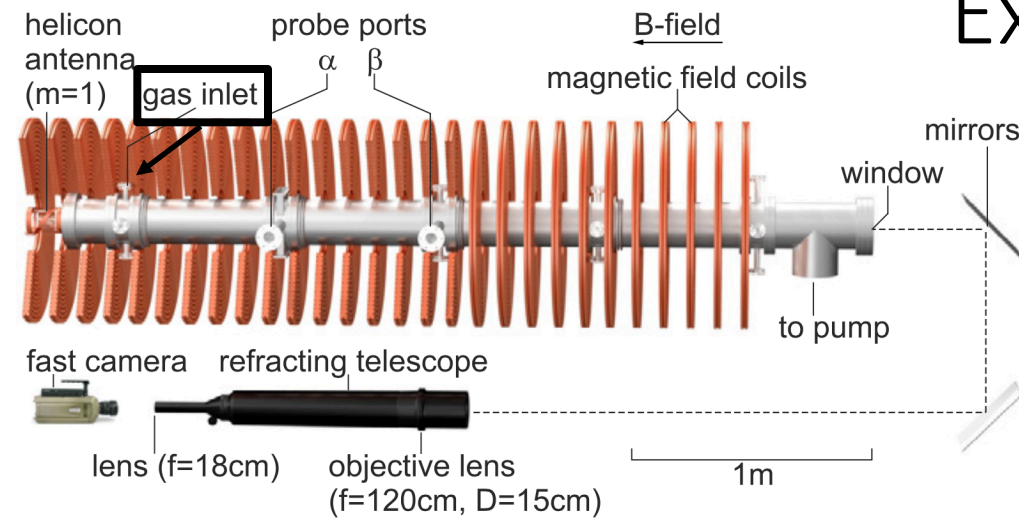
# Outline

- Background:
  - Linear Device Configuration and Results: CSDX & PANTA
  - Problem: Origin of axial flow?
- Review of intrinsic rotation
  - Residual stress, with applicability of conventional wisdom
- Dynamical Symmetry Breaking Mechanism
  - Dynamical symmetry breaking
  - Compare to standard mechanism: negative viscosity vs intrinsic torque
- Negative Viscosity Phenomena
  - Modulational instability for a test flow shear  $\delta\langle v_z \rangle' \leftrightarrow \chi_\phi$  vs  $|\chi^{Res}|$
  - What stops  $\langle v_z \rangle'$  growth? – Parallel Shear Flow Instability (PSFI)
- Flow structure
  - Turbulent pipe flow model:  $\Delta P_z$ , neutral boundary layer
  - Flow profile: Including PSFI effect  $\rightarrow \langle v_z \rangle'$  structure
- Significance for tokamaks
- Conclusion

# Summary

- **Intrinsic flow** suggested by experiments in linear devices, where conventional wisdom does not apply
- Dynamical symmetry breaking: Seeded by test flow shear  $\delta\langle v_z \rangle' \rightarrow$  Intrinsic flow  $\rightarrow \delta\langle v_z \rangle'$  feeds back on itself
- Perturbed residual stress  $\delta\Pi^{Res} \sim |\chi^{Res}|\delta\langle v_z \rangle'$  induces **negative viscosity increment**  $|\chi^{Res}|$ , total viscosity  $\chi_\phi^{tot} = \chi_\phi - |\chi^{Res}|$
- Flow shear  $\langle v_z \rangle'$  stays below Parallel Shear Flow Instability threshold; total viscosity stays positive
- For tokamaks: synergy of standard residual stress driven by  $\nabla T, \nabla P$ , etc. and  $\delta\Pi^{Res}$  induced negative viscosity increment

# Experiments: configuration



- CSDX<sup>[1]</sup>
- Gas input from side
- No axial momentum input

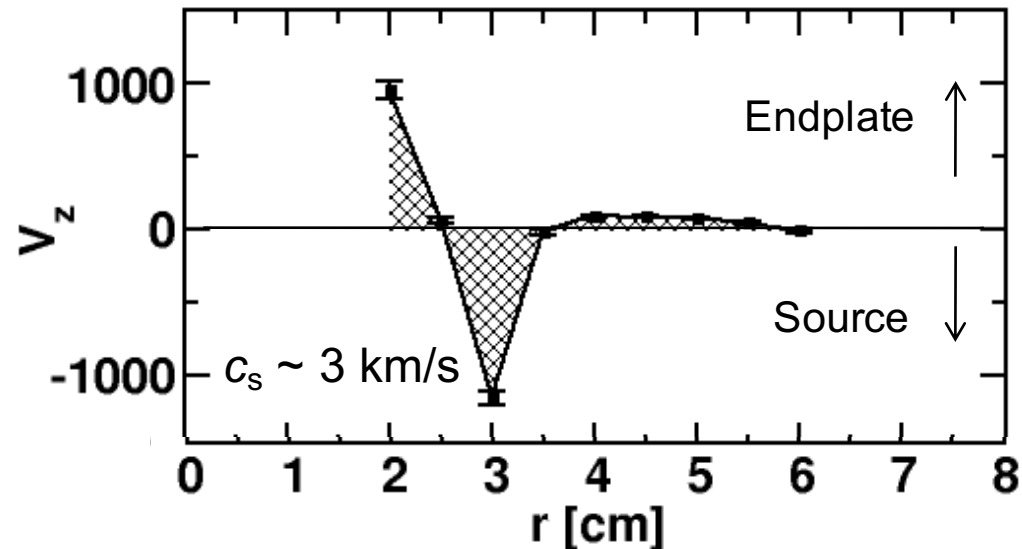
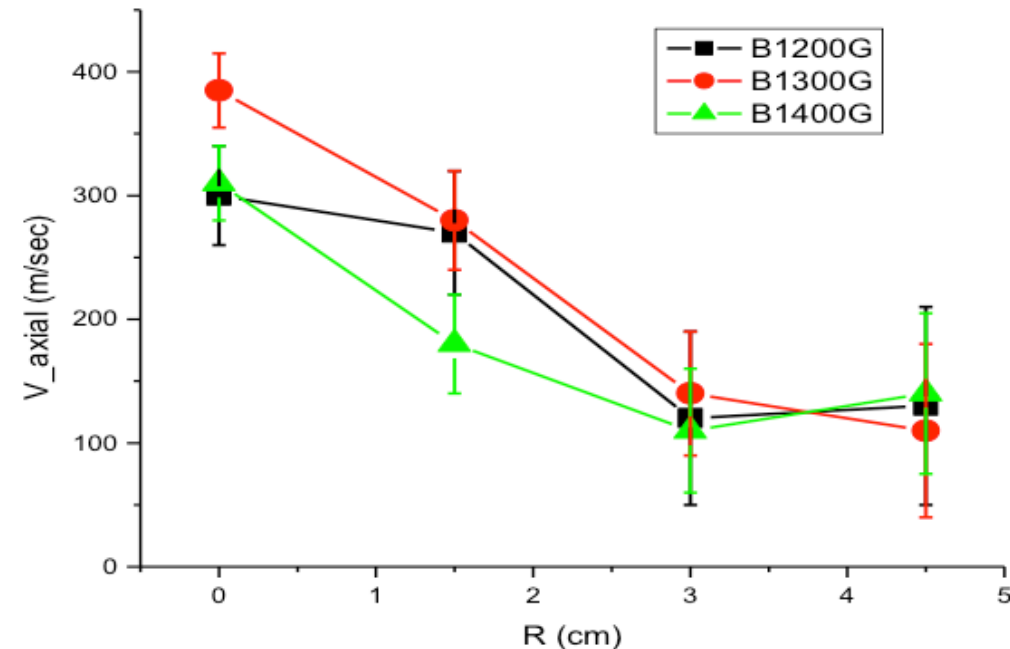
- PANTA<sup>[2]</sup>
- Gas input from the source end
- Axial momentum input

Parameters	CSDX Typical Values	PANTA Typical Values
Source	< 5 kW	3 kW
Pressure	0.1~1.3 Pa	0.1 Pa, 0.4 Pa
<b>B</b> field	Up to 2400 G	900 G
$T_e$	3~6 eV	3 eV
$n_e$	$0.5 \sim 2 \times 10^{19} \text{ m}^{-3}$	$1 \times 10^{19} \text{ m}^{-3}$
$T_i$	0.3~0.8 eV	---

\* [1] S. Thakur et al, Plasma Sources Sci. Technol. **23** (2014) 044006;

[2] T. Kobayashi (2014, Jun). *Parallel flow structure formation by turbulent momentum transport in linear magnetized plasma*. Asia Pacific Transport Working Group, Kyushu University, Japan.

# Profile of Axial Flow



- CSDX<sup>[1]</sup>
- No axial momentum input
- Flow profile steepens as B increases

- PANTA<sup>[2]</sup>
- Flow reversal
- Input flow: insufficient momentum input

Intrinsic axial flow!

Origin, physics?

\* [1] L. Cui (2015, Nov). *Spontaneous Profile Self-Organization in a Simple Realization of Drift-Wave Turbulence*. Invited talk, Session BI3, 57<sup>th</sup> APS-DPP meeting, Savannah, Georgia.

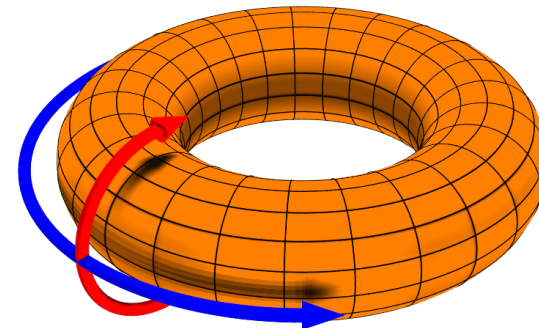
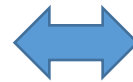
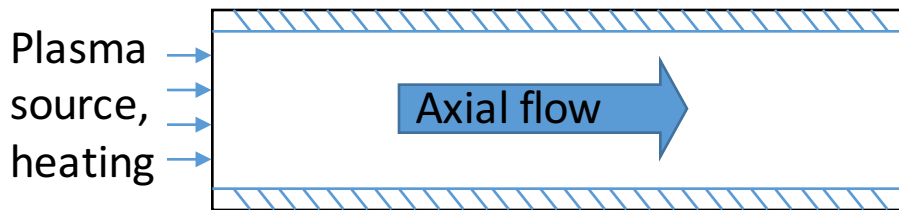
[2] T. Kobayashi (2014, Jun). *Parallel flow structure formation by turbulent momentum transport in linear magnetized plasma*. Asia Pacific Transport Working Group, Kyushu University, Japan.

# Evidence of Intrinsic Flow

Device	Cause of Driven Flow	Evidence of Intrinsic Flow
CSDX	<p>Neutral gas</p> <ul style="list-style-type: none"> <li>→ Ionized &amp; heated during helicon discharge</li> <li>→ Ion pressure gradient in axial direction <math>\Delta P_z</math></li> <li>→ Driven flow</li> </ul>	<p>Flow profile, density profile steepen as <math>B</math> increases:</p> <p><math>\nabla N \uparrow \rightarrow</math> Drift Wave (DW) turbulence <math>\uparrow</math></p> <ul style="list-style-type: none"> <li>→ Turbulent transport of axial momentum <math>\uparrow</math></li> <li>→ Intrinsic flow interacts with driven flow</li> <li>→ Total flow structure changes</li> </ul>
PANTA	<p>Gas thruput into the source end</p> <ul style="list-style-type: none"> <li>→ External momentum source</li> <li>→ Drives flow from source to endplate</li> </ul>	<p>Flow reversal</p> <ul style="list-style-type: none"> <li>→ Intrinsic flow interacts with driven flow</li> <li>→ Global net flow direction: Source <math>\rightarrow</math> Endplate</li> </ul>

# Problem

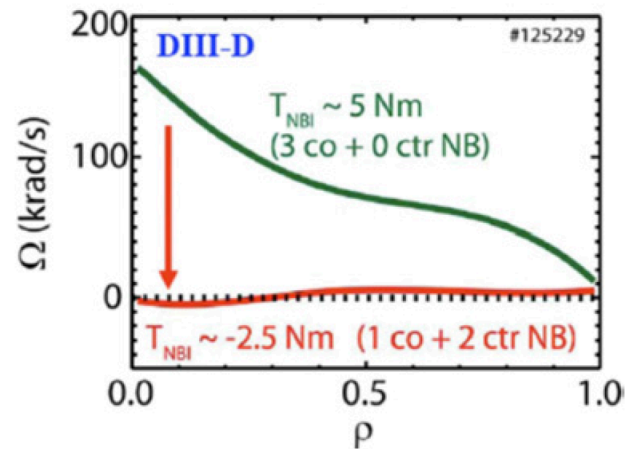
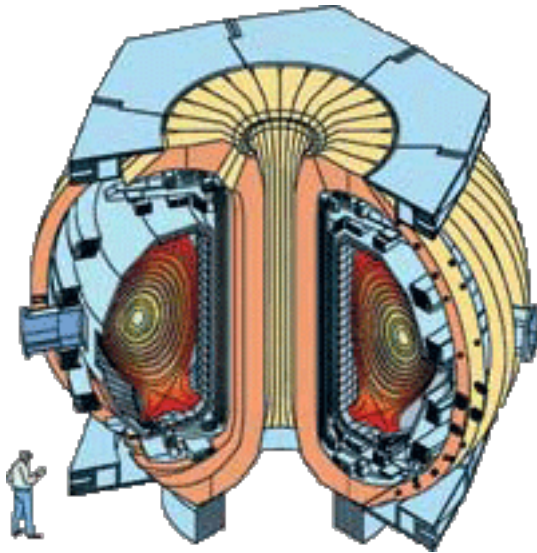
- Axial flows
  - CSDX, PANTA both suggest the existence of intrinsic axial flows
- Questions:
  - (1) What generates the intrinsic flow?
  - (2) How does intrinsic flow interact with driven flow?
- Clue:
  - Analogous to intrinsic rotation in tokamaks: axial  $\leftrightarrow$  parallel



Parallel flow

# Intrinsic Rotation in Tokamaks

- Cancellation experiment: existence of intrinsic torque
- Neutral Beam Injection (NBI)  $\rightarrow$  Heating, external torque
- 1 co + 2 ctr  $\rightarrow$  0 total  $\rightarrow$  Intrinsic torque = 1 co NB



**Figure 1.** ‘Cancellation’ experiment of Solomon *et al* from DIII-D [21]. A mix of 1 co and 2 counter beams yield a flat rotation profile with  $\langle v_\phi \rangle \cong 0$ . This shows that the intrinsic torque for these parameters is approximately that of 1 neutral beam, in the co-current direction.



# Standard Approach

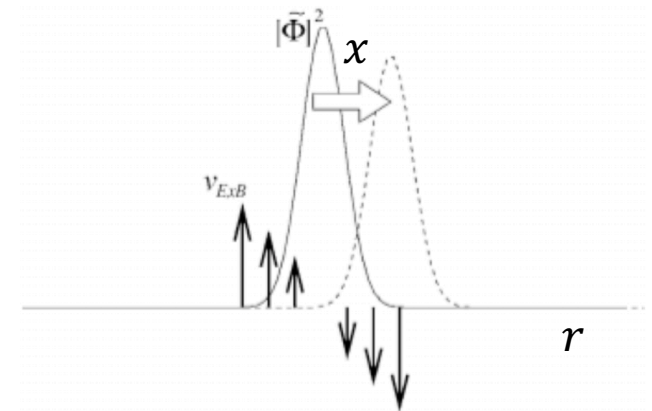
- Mean flow equation:

$$\partial_t \langle v_{\parallel} \rangle + \partial_r \langle \tilde{v}_r \tilde{v}_{\parallel} \rangle = 0$$

- Intrinsic flow is accelerated by the residual piece of the momentum flux:

$$\langle \tilde{v}_r \tilde{v}_{\parallel} \rangle = -\chi_{\phi} \frac{d \langle v_{\parallel} \rangle}{dr} + V_P \langle \tilde{v}_{\parallel} \rangle + \Pi_{r\parallel}^{Res}$$

- Ignore momentum pinch  $V_P$
- Correlated by  $\mathbf{B}$  field structure,  $k_{\parallel} = k_{\theta} \frac{x}{L_S}$ ,  $L_S =$  magnetic shear length
- $\Pi_{r\parallel}^{Res} \sim \langle k_{\theta} k_{\parallel} \rangle = \sum_k k_{\theta} k_{\parallel} |\phi_k|^2 = k_{\theta}^2 \frac{\langle x \rangle}{L_S}$ 
  - $x$  : distance from rational surface
- Needs symmetry breaking!



# Symmetry Breaking

- Summary of conventional symmetry breaking mechanisms\*:

Conventional mechanisms	Key physics
Electric field shear $E_r'$	Centroid shift $\rightarrow$ parallel acoustic wave asymmetry $\rightarrow$ mean $\langle k_{\parallel} \rangle$
Intensity gradient $I'$	Spectral dispersion from intensity gradient
Stress from polarization acceleration $\langle \tilde{E}_{\parallel} \nabla_{\perp}^2 \tilde{\phi} \rangle$	Guiding center stress from acceleration due to polarization charge
Stress from $\partial_r \langle \tilde{v}_r \tilde{v}_{\perp} \rangle \rightarrow B_{\theta} \langle J_r \rangle$	$\mathbf{J} \times \mathbf{B}$ torque from polarization flux

- Preference of wave propagation in parallel direction,  $\langle k_{\parallel} \rangle \neq 0$
- Do not apply to CSDX or PANTA  $\leftarrow$  Straight  $\mathbf{B}$  fields

~~$$k_{\parallel} = k_{\theta} \frac{x}{L_s}$$~~

\* P.H. Diamond et al, Nucl. Fusion 53 (2013) 104019;  
 P.H. Diamond et al, Nucl. Fusion 49 (2009) 045002.

# Summary of Conventional Wisdom

- Intrinsic flow accelerated by  $\Pi_{r\parallel}^{Res} \sim \langle k_\theta k_\parallel \rangle$ 
  - Needs symmetry breaking
- Standard approach
  - Intrinsic torque,  $-\partial_r \Pi_{r\parallel}^{Res}$  accelerates flow
  - Does **NOT** apply to straight **B** fields
- Dynamical Symmetry Breaking
  - Drift wave turbulence in presence of axial flow shear
  - $\delta \langle v_z \rangle'$  seeds symmetry breaking
  - Negative viscosity increment

# Model Equations

- Hasegawa-Wakatani + Axial flow:

$$\frac{D}{Dt}(1 - i\delta - \nabla_{\perp}^2)\phi + \frac{1}{L_n} \frac{1}{r} \frac{\partial \phi}{\partial \theta} + \boxed{\frac{\partial v_z}{\partial z}} = 0,$$

$$\frac{D}{Dt}v_z - \langle v_z \rangle' \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -(1 - i\delta) \frac{\partial \phi}{\partial z},$$

Acoustic coupling

- Acoustic coupling

- Couple axial flow fluctuation to DW
- Familiar: Convert parallel compression into zonal flow\*

- $i\delta$ : nonadiabatic electron response  $\rightarrow$  Drift wave instability

- Dispersion relation:  $1 + k_{\perp}^2 \rho_s^2 - i\delta - \frac{\omega_*}{\omega} + \frac{\boxed{k_{\theta} k_z \rho_s c_s \langle v_z \rangle'}}{\omega^2} - (1 - i\delta) \frac{k_z^2 c_s^2}{\omega^2} = 0.$

Drift wave

Symmetry breaking

Ion acoustic wave

# Dynamical Symmetry Breaking

- Growth rate  $\sim$  frequency shift:

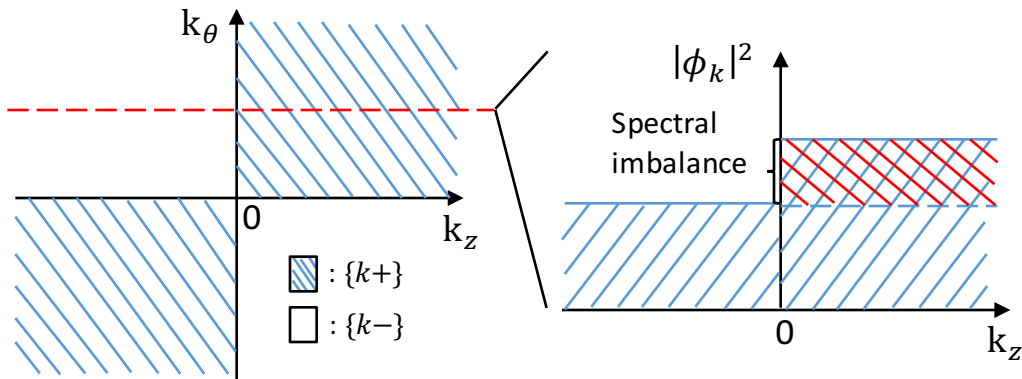
$$\gamma_k \cong \frac{\nu_{ei}}{k_z^2 v_{The}^2} \frac{\omega_* (\omega_* - \omega_k)}{(1 + k_\perp^2 \rho_s^2)^2}$$

- Frequency:

$$\omega_k \cong \frac{\omega_*}{1 + k_\perp^2 \rho_s^2} - \frac{k_\theta k_z \rho_s c_s \langle v_z \rangle'}{\omega_*}$$

- Frequency shift  $\sim$  Flow shear:

$$\gamma_k \cong \frac{\nu_{ei}}{k_z^2 v_{The}^2} \frac{\omega_*^2}{(1 + k_\perp^2 \rho_s^2)^2} \left( \frac{k_\perp^2 \rho_s^2}{1 + k_\perp^2 \rho_s^2} + \frac{k_\theta k_z \rho_s c_s \langle v_z \rangle'}{\omega_*^2} \right)$$



$\{k_\pm\}$ : Domains where modes grow faster/slower

Fig. 1: Spectral imbalance.

- Spectral imbalance:

Infinitesimal test axial flow shear, e.g.  $\delta \langle v_z \rangle' > 0$

Modes with  $k_\theta k_z > 0$  grow faster than other modes,

$$\gamma_k |_{k_\theta k_z > 0} > \gamma_k |_{k_\theta k_z < 0}$$

Spectral imbalance (Fig. 1)

$$\langle k_\theta k_z \rangle > 0 \rightarrow \Pi_{rZ}^{Res} \neq 0$$

# Quasilinear Reynolds Stress

- Reynolds stress = diffusive flux + residual stress

$$\langle \tilde{v}_r \tilde{v}_z \rangle = \Re \sum_k \frac{i}{\omega} (k_\theta k_z \rho_s c_s - k_\theta^2 \rho_s^2 \langle v_z \rangle') |\phi_k|^2 + \sum_k \frac{\delta}{\omega} k_\theta k_z \rho_s c_s |\phi_k|^2 = -\chi_\phi \langle v_z \rangle' + \Pi_{rz}^{\text{Res}}$$

- Turbulent diffusivity:  $\chi_\phi = \sum_k \frac{\nu_{ei}}{k_z^2 v_{\text{The}}^2} \frac{k_\perp^2 \rho_s^2}{1 + k_\perp^2 \rho_s^2} k_\theta^2 \rho_s^2 |\phi_k|^2$

- Residual stress:  $\Pi_{rz}^{\text{Res}} = \sum_k \left( \frac{\gamma_k}{\omega_k^2} + \frac{\delta}{\omega_k} \right) k_\theta k_z \rho_s c_s |\phi_k|^2$   
 $= \sum_k \frac{\nu_{ei}}{k_z^2 v_{\text{The}}^2} (2 + k_\perp^2 \rho_s^2) \left[ \frac{k_\perp^2 \rho_s^2}{1 + k_\perp^2 \rho_s^2} + \frac{k_\theta k_z \rho_s c_s \langle v_z \rangle'}{\omega_*^2} \right] k_\theta k_z \rho_s c_s |\phi_k|^2$

- Sum over 2 domains, accounting for the spectral imbalance

$$\Pi_{rz}^{\text{Res}} = \text{Sign}(\delta \langle v_z \rangle') \sum_{\{k+\}} \frac{\nu}{k_\parallel^2 v_{\text{The}}^2} (2 + k_\perp^2 \rho_s^2) \frac{k_\perp^2 \rho_s^2}{1 + k_\perp^2 \rho_s^2} |k_y k_\parallel| \rho_s c_s \underbrace{\Delta I_k(\delta \langle v_z \rangle')}_{\updownarrow}$$

$$\Delta I_k(\delta \langle v_z \rangle') \equiv |\phi_k|^2|_{\{k+\}} - |\phi_k|^2|_{\{k-\}} \longleftrightarrow \boxed{\text{Spectral imbalance} \sim \delta \langle v_z \rangle'}$$

# Contrast the 2 Stories

	Standard Symmetry Breaking	Dynamical Symmetry Breaking
Free energy source	$\nabla T_i, \nabla n, \dots$ depending on turbulence type	Only drift wave turbulence so far, $\nabla n$
Symmetry breaker	Radial electric field shear, $E_r'$ ; Intensity gradient, $I(x)'$ , etc. All tied to magnetic field configuration.	Test axial flow shear, $\delta\langle v_z \rangle'$ ; No requirement for shear of $\mathbf{B}$ structure.
Effect on the flow	Intrinsic torque, $-\partial_r \Pi_{r\parallel}^{Res}$	Negative viscosity, $\delta \Pi_{rz}^{Res} =  \chi^{Res}  \delta\langle v_z \rangle'$
Flow profile	$\langle v_{\parallel} \rangle' = \frac{\Pi_{r\parallel}^{Res}}{\chi_{\phi}}$	$\langle v_z \rangle' = \frac{\text{Flow drive } (\Pi_{rz}^{Res}, \Delta P_z)}{\chi_{\phi} -  \chi^{Res} }$
Feedback loop		

# Negative Viscosity Increment

- Calculate negative diffusion  $\delta\Pi_{rz}^{Res} \sim |\chi^{Res}| \delta\langle v_z \rangle'$ , back-of-envelope style
- Quasilinear residual stress:  $\Pi_{rz}^{Res} \sim \sum_k \frac{\gamma_k}{\omega_k} k_\theta k_z \rho_s c_s N_k$
- $N_k \sim |\phi_k|^2 / \omega_k$  wave action density governed by wave kinetic equation:

$$\frac{\partial}{\partial t} N + v_{gr} \frac{\partial}{\partial r} N - \frac{\partial}{\partial r} (\omega_k + \mathbf{k} \cdot \mathbf{V}) \frac{\partial}{\partial k_r} N = \gamma_k N - \Delta\omega_k \frac{N^2}{N_0}$$

Convection by wave packet
Refraction
Linear growth
Self-interaction

$$\Rightarrow \delta N_k \sim \tau_c \delta\gamma_k N_k \sim \gamma_k^{-1} \delta\gamma_k N_k$$

- Recall:  $\gamma_k \cong \frac{\nu_{ei}}{k_z^2 v_{The}^2} \frac{\omega_*^2}{(1 + k_\perp^2 \rho_s^2)^2} \left( \frac{k_\perp^2 \rho_s^2}{1 + k_\perp^2 \rho_s^2} + \frac{k_\theta k_z \rho_s c_s \langle v_z \rangle'}{\omega_*^2} \right) \Rightarrow \delta\gamma_k = \frac{\nu_{ei}}{k_z^2 v_{The}^2} \frac{k_\theta k_z \rho_s c_s}{(1 + k_\perp^2 \rho_s^2)^2} \delta\langle v_z \rangle'$

$$\Rightarrow \delta\Pi_{rz}^{Res} \sim \frac{\nu_{ei} L_n^2}{v_{the}^2} \sum_k |\phi_k|^2 \delta\langle v_z \rangle' \sim |\chi^{Res}| \delta\langle v_z \rangle'$$



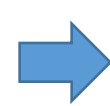
# Negative Viscosity Increment: cont'd

- Dynamics of a test flow shear

$$\frac{\partial}{\partial t} \delta \langle v_z \rangle' + \frac{\partial^2}{\partial r^2} (\delta \Pi_{rz}^{\text{Res}} - \chi_\phi \delta \langle v_z \rangle') = 0$$

$$\delta \Pi_{rz}^{\text{Res}} = \frac{\nu_{ei} L_n^2}{v_{\text{The}}^2} \sum_k (1 + k_\perp^2 \rho_s^2) (4 + k_\perp^2 \rho_s^2) |\phi_k|^2 \delta \langle v_z \rangle' = |\chi^{\text{Res}}| \delta \langle v_z \rangle'$$

(From formal calculation)

  $\frac{\partial}{\partial t} \delta \langle v_z \rangle' - \frac{\partial^2}{\partial r^2} (\chi_\phi - |\chi^{\text{Res}}|) \delta \langle v_z \rangle' = 0$

- Negative viscosity increment:

$$|\chi^{\text{Res}}| = \nu_{ei} L_n^2 / v_{\text{The}}^2 \sum_k (1 + k_\perp^2 \rho_s^2) (4 + k_\perp^2 \rho_s^2) |\phi_k|^2$$

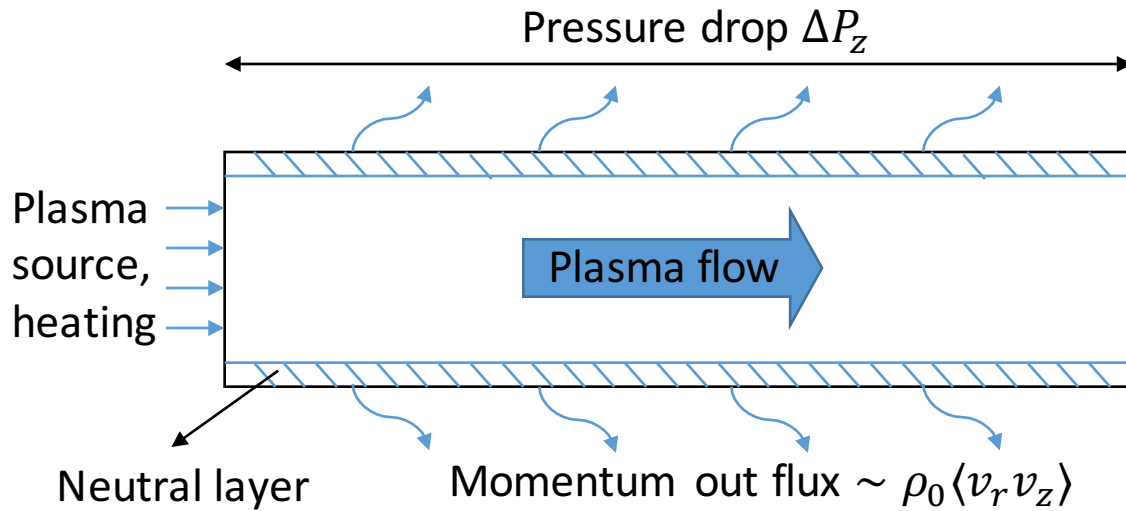
- Growth rate of flow shear modulation

$$\gamma_q = -q_r^2 (\chi_\phi - |\chi^{\text{Res}}|)$$

# Limits on $\langle v_z \rangle'$

- $\chi_\phi^{\text{tot}} = \chi_\phi - |\chi^{\text{Res}}| < 0 \rightarrow \delta \langle v_z \rangle'$  grows, profile steepens, until...
- $\langle v_z \rangle'$  hits Parallel Shear Flow Instability (PSFI) threshold
  - PSFI: recall dispersion relation of the model with adiabatic electrons:
 
$$(1 + k_\perp^2 \rho_s^2) \omega^2 - \omega_* \omega + k_\theta k_z \rho_s c_s \langle v_z \rangle' - k_z^2 c_s^2 = 0$$
  - Unstable  $\leftrightarrow$  discriminant  $\equiv \omega_*^2 - 4(1 + k_\perp^2 \rho_s^2)(k_\theta k_z \rho_s c_s \langle v_z \rangle' - k_z^2 c_s^2) < 0$
  - $\rightarrow \langle v_z \rangle' > \langle v_z \rangle'_{\text{crit}} \equiv \frac{1}{k_\theta k_z \rho_s c_s} \left[ \frac{\omega_*^2}{4(1 + k_\perp^2 \rho_s^2)} + k_z^2 c_s^2 \right] \rightarrow \text{PSFI}$
- PSFI turbulence  $\rightarrow \chi_\phi^{\text{PSFI}}$  adds on to the ambient  $\chi_\phi^{\text{tot}}$ 
  - $\rightarrow \chi_\phi^{\text{tot}} = \chi_\phi^{\text{DW}} + \chi_\phi^{\text{PSFI}} \Theta(\langle v_z \rangle' - \langle v_z \rangle'_{\text{crit}}) - |\chi^{\text{Res}}|$
- $\chi_\phi^{\text{PSFI}}$  switched on,  $\chi_\phi^{\text{PSFI}} > |\chi^{\text{Res}}| \rightarrow \chi_\phi^{\text{tot}} > 0$
- $\langle v_z \rangle'$  stays below PSFI threshold; total viscosity stays positive.
- Similar to nonlinear damping of zonal flow

# Flow Structure in Linear Device



	Pipe flow	Plasma flow
Drive	Pressure drop $\Delta P_z$	Ion pressure drop $\Delta P_z$
Boundary condition	No slip	Set by neutral layer
Viscosity	$\nu$	$\chi_\phi -  \chi^{Res} $

- Idea of Model: Turbulent pipe flow, Prandtl + Residual Stress
- Prandtl (momentum balance):  $\pi R^2 \Delta P_z = 2\pi R L_z \rho_0 \langle v_r v_z \rangle$
- Reynolds stress:  $\langle v_r v_z \rangle = -(\chi_\phi - |\chi^{Res}|) \langle v_z \rangle'$
- $\rightarrow$  Flow profile:  $\langle v_z \rangle' = -\frac{R \Delta P_z}{2L_z \rho_0 (\chi_\phi - |\chi^{Res}|)}$

# Flow Structure: cont'd

- PSFI  $\rightarrow$  Enhance turbulent diffusion,

$$\chi_{\phi}^{\text{eff}} = \chi_{\phi}^{\text{DW}} + \chi_{\phi}^{\text{PSFI}} \Theta(\langle v_z \rangle' - \langle v_z \rangle'_{\text{crit}})$$

- Including PSFI effect:

$$\langle v_z \rangle' = - \frac{R \Delta P_z}{2L_z \rho_0 \left[ \chi_{\phi}^{\text{DW}} + \chi_{\phi}^{\text{PSFI}} \Theta(\langle v_z \rangle' - \langle v_z \rangle'_{\text{PSFI}}) - |\chi^{\text{Res}}| \right]}$$

- $\chi_{\phi}^{\text{PSFI}}$  nonlinear in  $\langle v_z \rangle' \rightarrow \chi_{\phi}^{\text{eff}} > |\chi^{\text{Res}}| \rightarrow$  Profile relaxes
- $\langle v_z \rangle'$  stays below PSFI threshold

# Implication for Tokamaks

- Synergy of  $\Pi^{Res}(\nabla T, \nabla P, \nabla N)$  and  $\delta\Pi^{Res} = |\chi^{Res}| \delta\langle v_z \rangle'$

- DW turbulence,  $\mathbf{B}$  shear
- Symmetry breaker  
( $E_r', I(x)', \dots$ )
- $\rightarrow$  residual stress  $\Pi_{r\parallel}^{Res}$



- DW turbulence
- Test flow shear
- $\rightarrow$  negative viscosity  $|\chi^{Res}|$



Applicable to  
electron DW's  
 $\rightarrow$  CTEM

- Flow profile set by momentum flux balance:

$$\langle v_r v_{\parallel} \rangle = - (\chi_{\phi} - |\chi^{Res}|) \frac{d\langle v_{\parallel} \rangle}{dr} + \Pi_{r\parallel}^{Res} = 0$$

- Enhanced flow profile

$$\frac{d\langle v_{\parallel} \rangle}{dr} = \frac{\Pi_{r\parallel}^{Res}}{\chi_{\phi} - |\chi^{Res}|}$$

$\rightarrow$  Mechanism to  
enhance intrinsic  
rotation predictions

# Conclusion

- Results from CSDX, PANTA suggest intrinsic axial flow;
- Intrinsic mechanism to generate axial flows and to build up a mean flow profile is introduced:
  - Test flow shear  $\delta\langle v_z \rangle'$  seeds symmetry breaking and feeds back on itself;
- Different from standard symmetry breaking mechanism:
  - Intrinsic torque  $-\partial_r \Pi^{Res}$  driven by  $\nabla T, \nabla P, \dots$  v.s. Negative viscosity increment  $|\chi^{Res}|$  induced by  $\delta \Pi^{Res}$ ;
- Flow structure in a linear device:  $\langle v_z \rangle' = -\frac{R\Delta P_z}{2L_z \rho_0 (\chi_\phi - |\chi^{Res}|)}$
- Implication for tokamaks:
  - Synergy of  $\Pi^{Res}(\nabla T, \nabla P, \dots)$  and  $\delta \Pi^{Res} = |\chi^{Res}| \delta \langle v_z \rangle'$ ;
  - Enhanced intrinsic rotation profile:  $\frac{d\langle v_{||} \rangle}{dr} = \frac{\Pi_{r||}^{Res}}{\chi_\phi - |\chi^{Res}|}$